

USE OF V_{s30} TO REPRESENT LOCAL SITE CONDITIONS

Presented by

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Presented at the Session 6 on

**The V_{s30} Dialog
How We Can & Cannot use V_{s30} in Site Response Estimation?**

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Effects OF Surface Geology on Strong Ground Motion
Santa Barbara, California
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Wave propagation theory suggests that ground motion amplitude should depend on the density and shear wave velocity, V_s , of the near surface material (e.g., Bullen, 1965; Aki & Richards, 1980). Density does not vary very much with depth; hence V_s becomes the logical choice for representing site conditions.

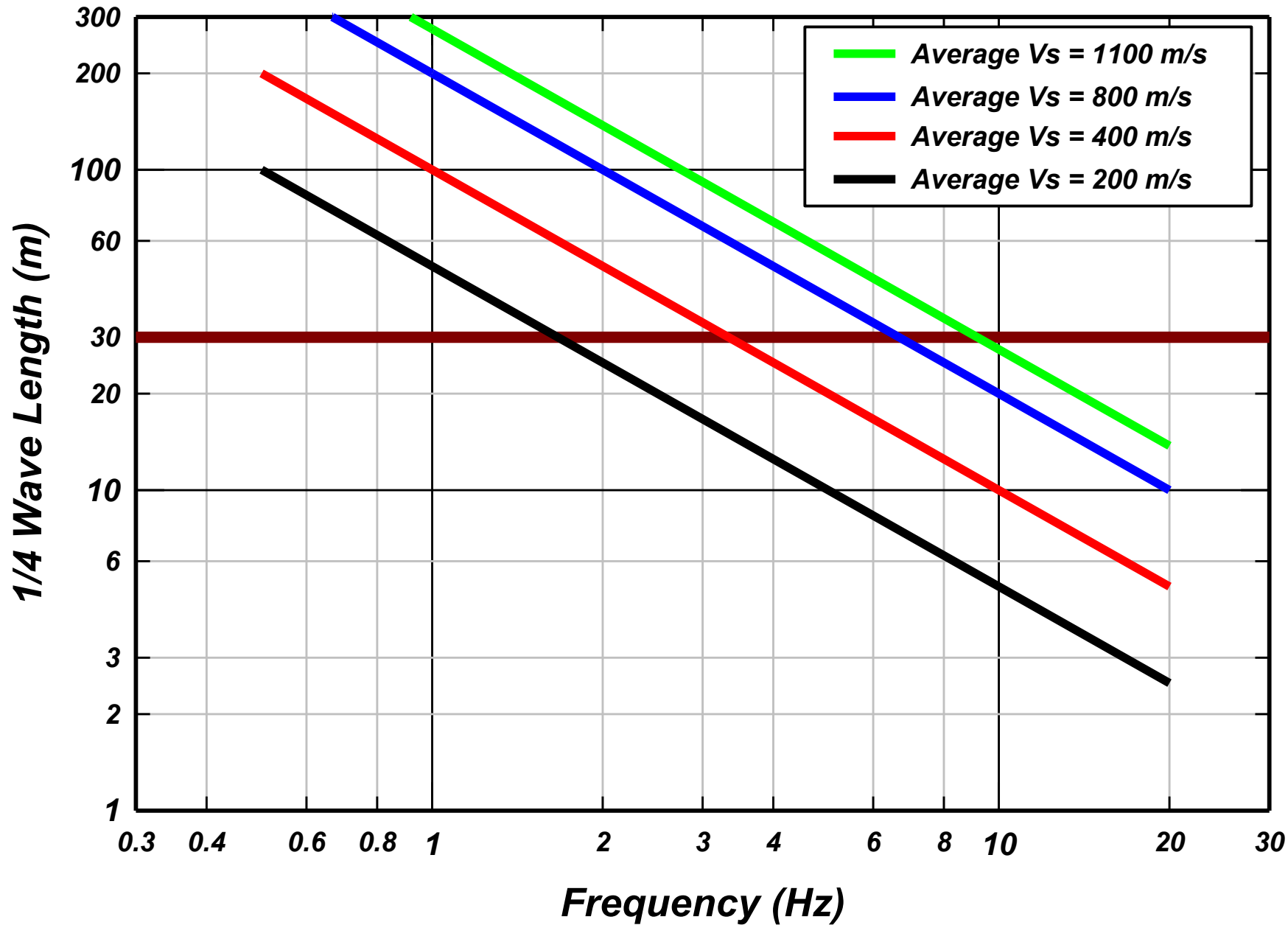
The essential issue then becomes in how to express this dependence.

***Two methods have been proposed over
the past 30 years.***



Method No. 1

1. The "average" velocity over the depth range corresponding to $\frac{1}{4}$ wavelength of the period of interest (Joyner et al, 1981).



Method No. 2

2. The use of V_{s30} (Borcherdt, 1994) , who recommended the use of $Vs30$ as a means for classifying Site Categories for building codes.

$$f_5(PGA_{1100}, V_{S30}^*) = a_{10} \text{Ln}\left(\frac{V_{S30}^*}{V_{LIN}}\right) - b \text{Ln}(PGA_{1100} + c) + b \text{Ln}\left[PGA_{1100} + c \text{Ln}\left(\frac{V_{S30}^*}{V_{LIN}}\right)^n\right] \quad \text{for } V_{S30} < V_{LIN}$$

$$f_5(PGA_{1100}, V_{S30}^*) = (a_{10} + bn) \text{Ln}\left(\frac{V_{S30}^*}{V_{LIN}}\right) \quad \text{for } V_{S30} \geq V_{LIN}$$

$$V_{S30}^* = V_{S30} \quad \text{for } V_{S30} < V_1$$

$$V_{S30}^* = V_1 \quad \text{for } V_{S30} \geq V_1$$

$$V_1 = 1500 \text{ m/s} \quad \text{for } T \leq 0.50 \text{ sec}$$

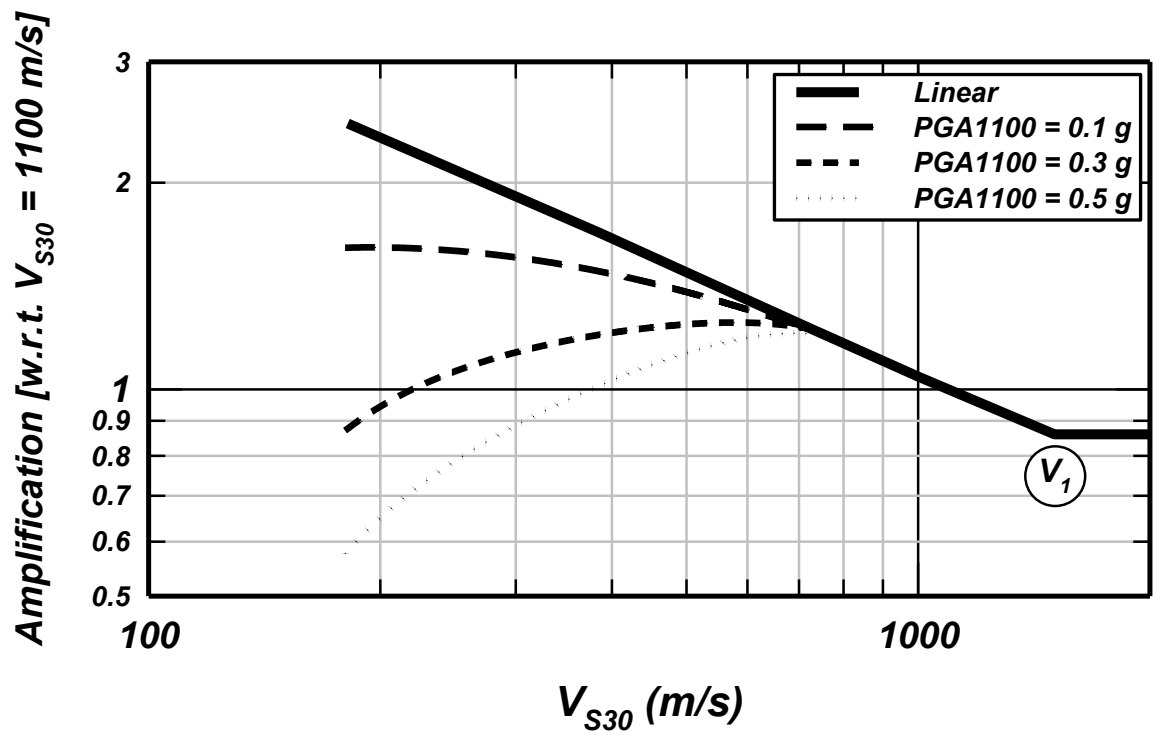
$$V_1 = \exp[8.0 - 0.795 \text{Ln}(T/0.21)] \quad \text{for } 0.50 \text{ sec} < T \leq 1 \text{ sec}$$

$$V_1 = \exp[6.76 - 0.297 \text{Ln}(T)] \quad \text{for } 1 \text{ sec} < T < 2 \text{ sec}$$

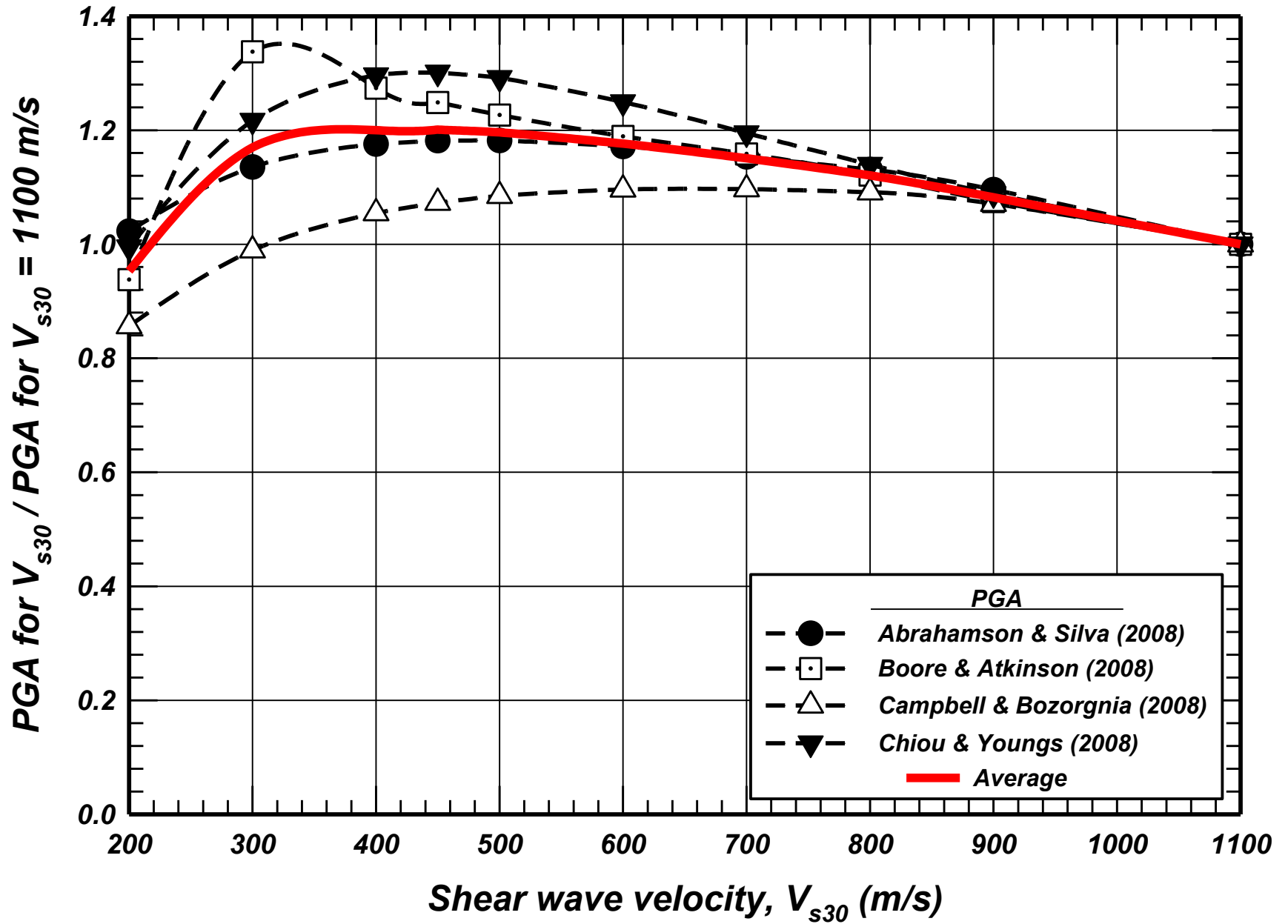
$$V_1 = 700 \text{ m/s} \quad \text{for } T \geq 2 \text{ sec}$$

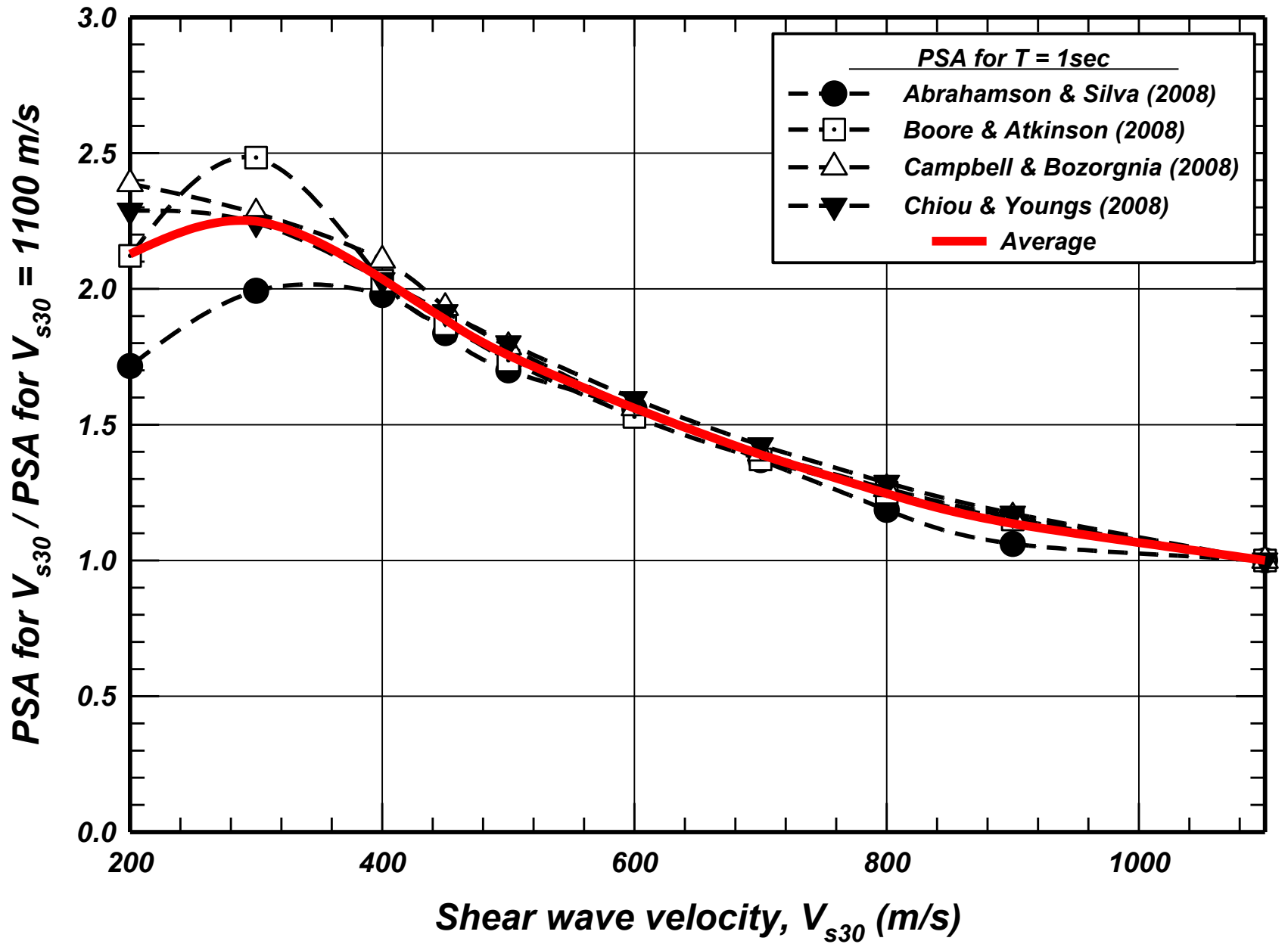
From Abrahamson & Silva (2008)

More recently, four of the five NGA relationships used V_{s30} as an independent parameter to explicitly represent local site conditions.



**Example of the V_{s30} scaling for $T = 0.2$ sec
From Abrahamson & Silva (2008)**

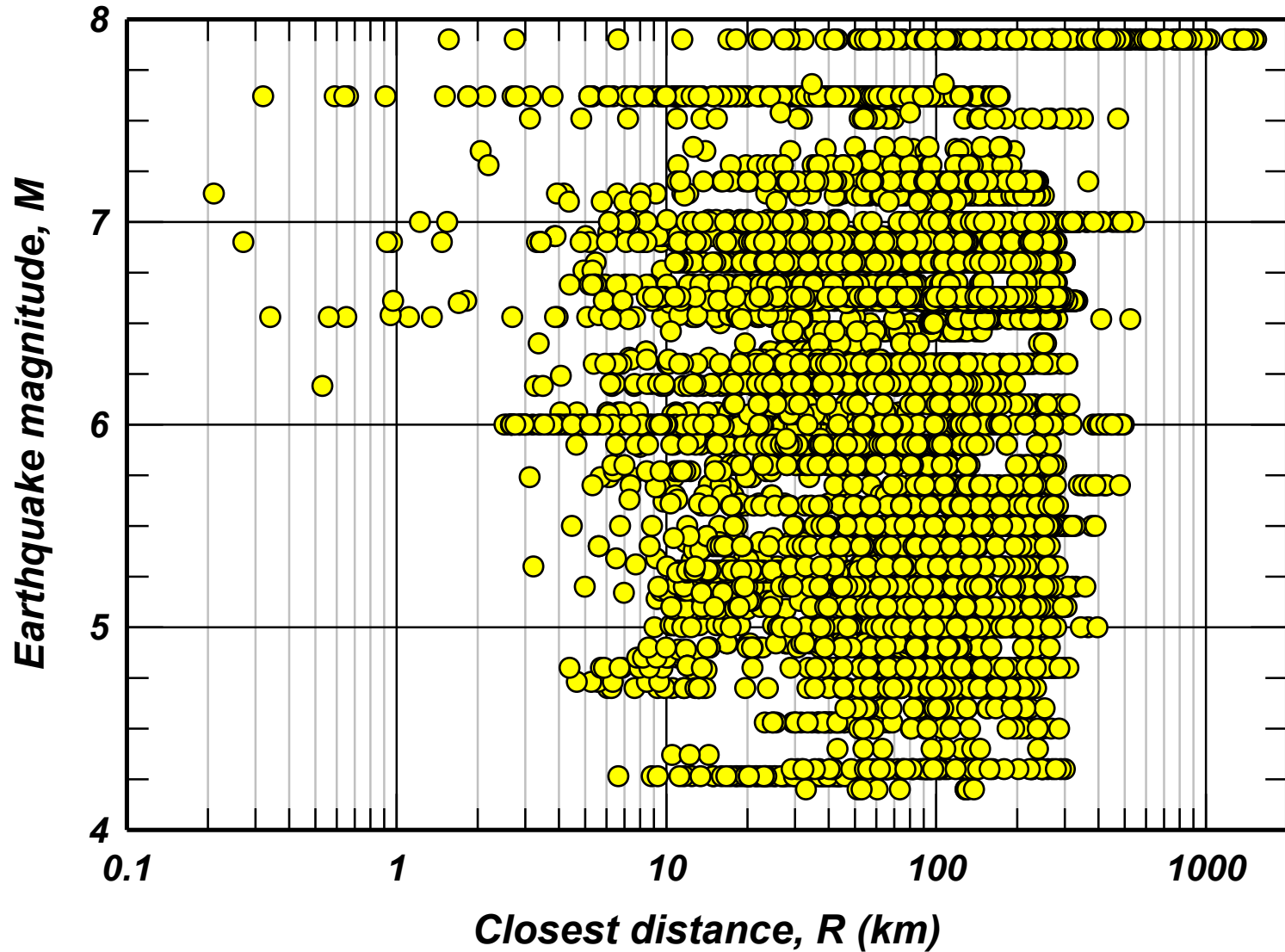




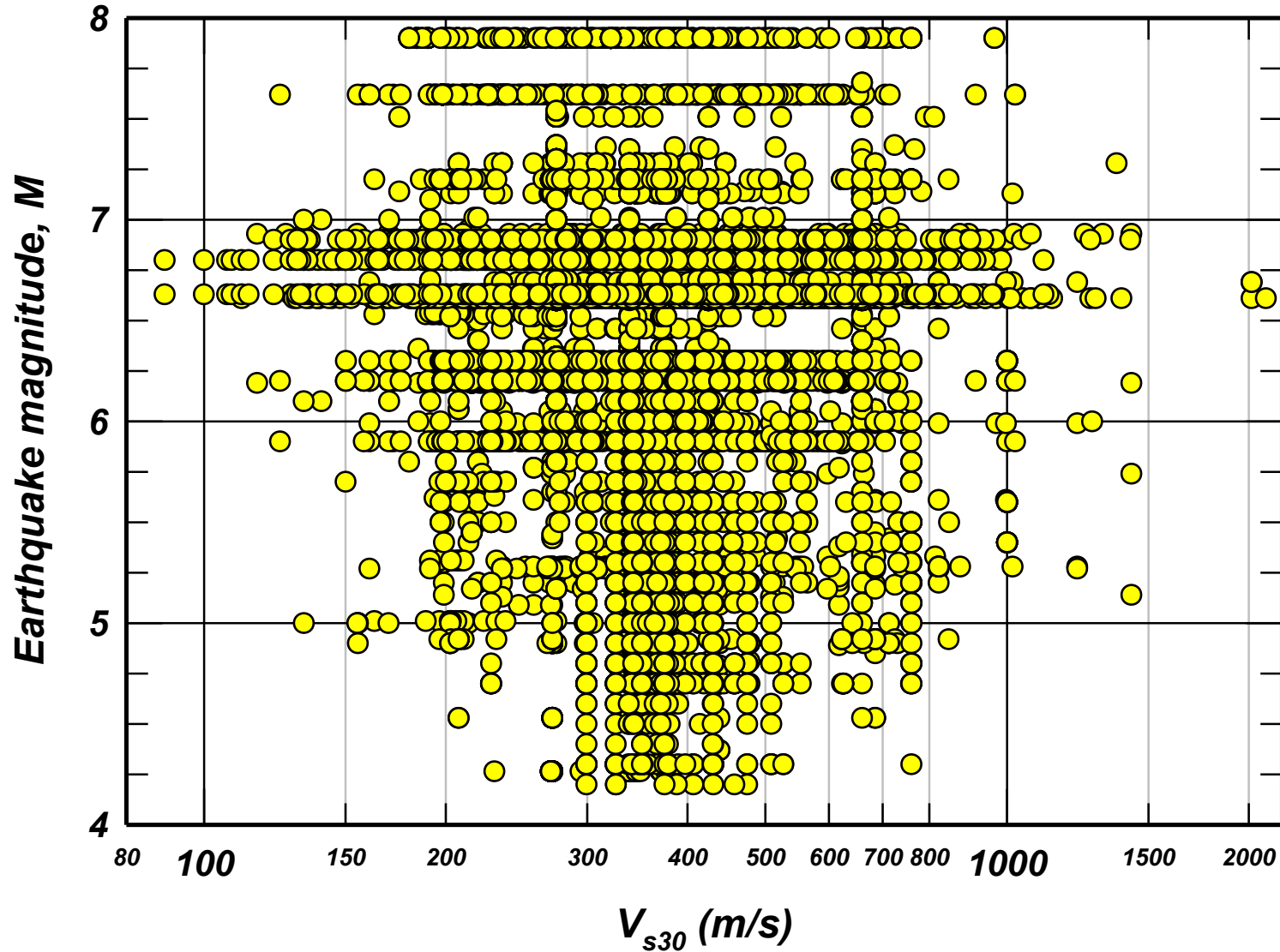
***NGA DATA
2011 FLATFILE***



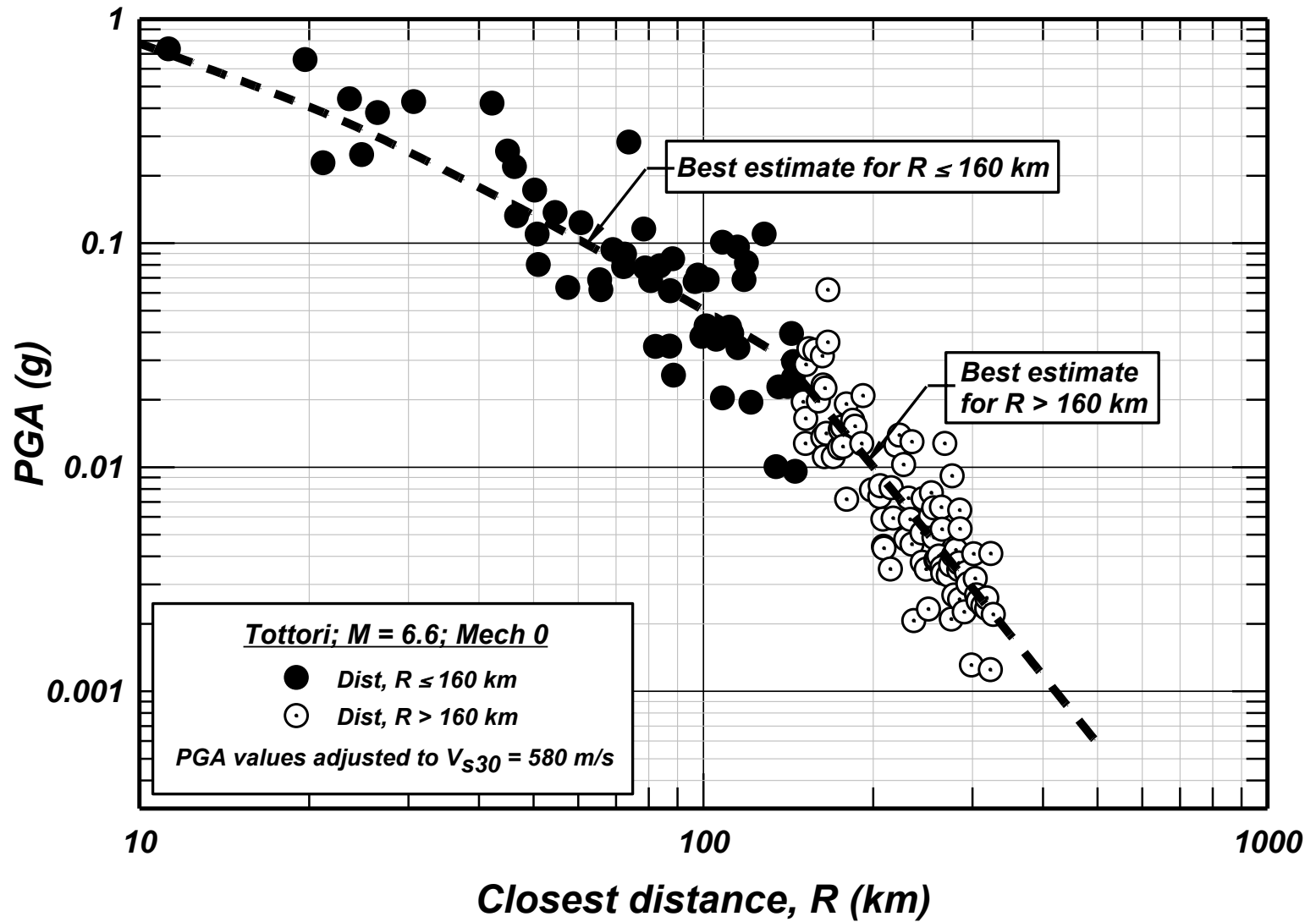
From Flatfile



From Flatfile



From Flatfile



Total No. of Entries

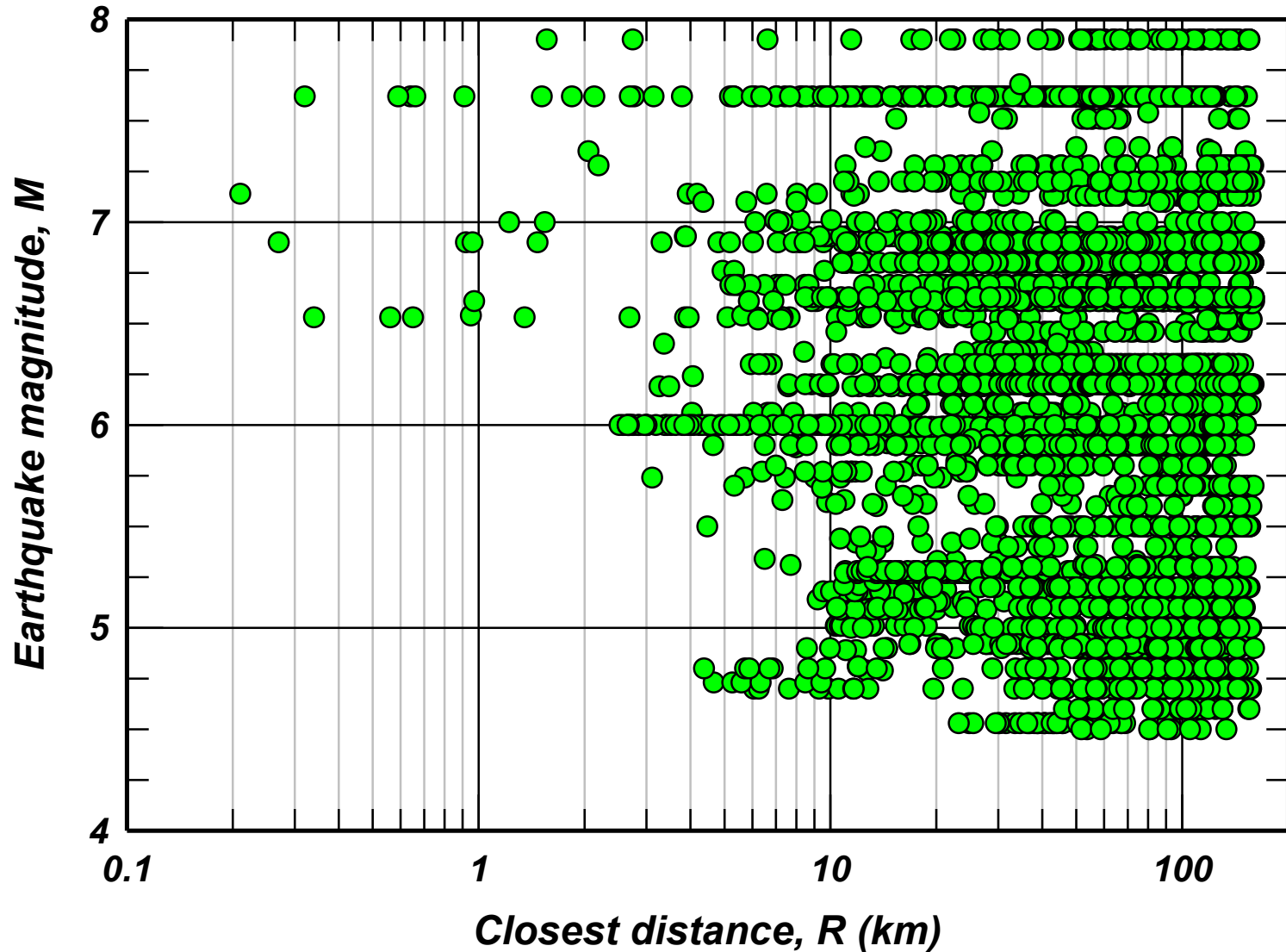
8163

<i>Non-FF</i>	426
<i>Mag not listed</i>	201
<i>Mechanism not listed</i>	139
<i>Distance not listed</i>	92
<i>Vs30 not listed</i>	17
<i>PSA not listed</i>	63
<i>Mag < 4.5</i>	173
<i>Distance > 160 km</i>	1890
<i>Others</i>	136

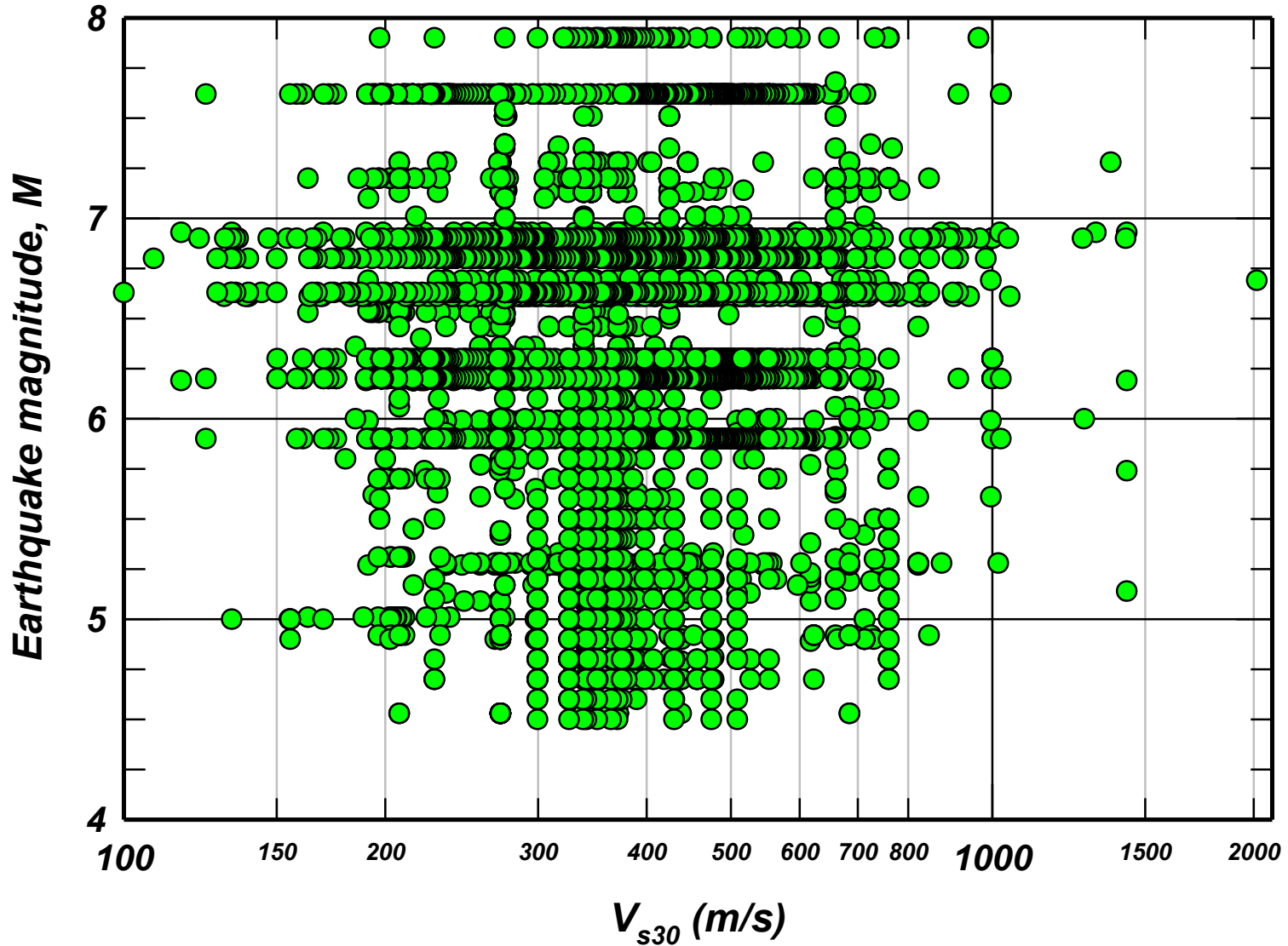
Total No. of FF Entries to be used

5026

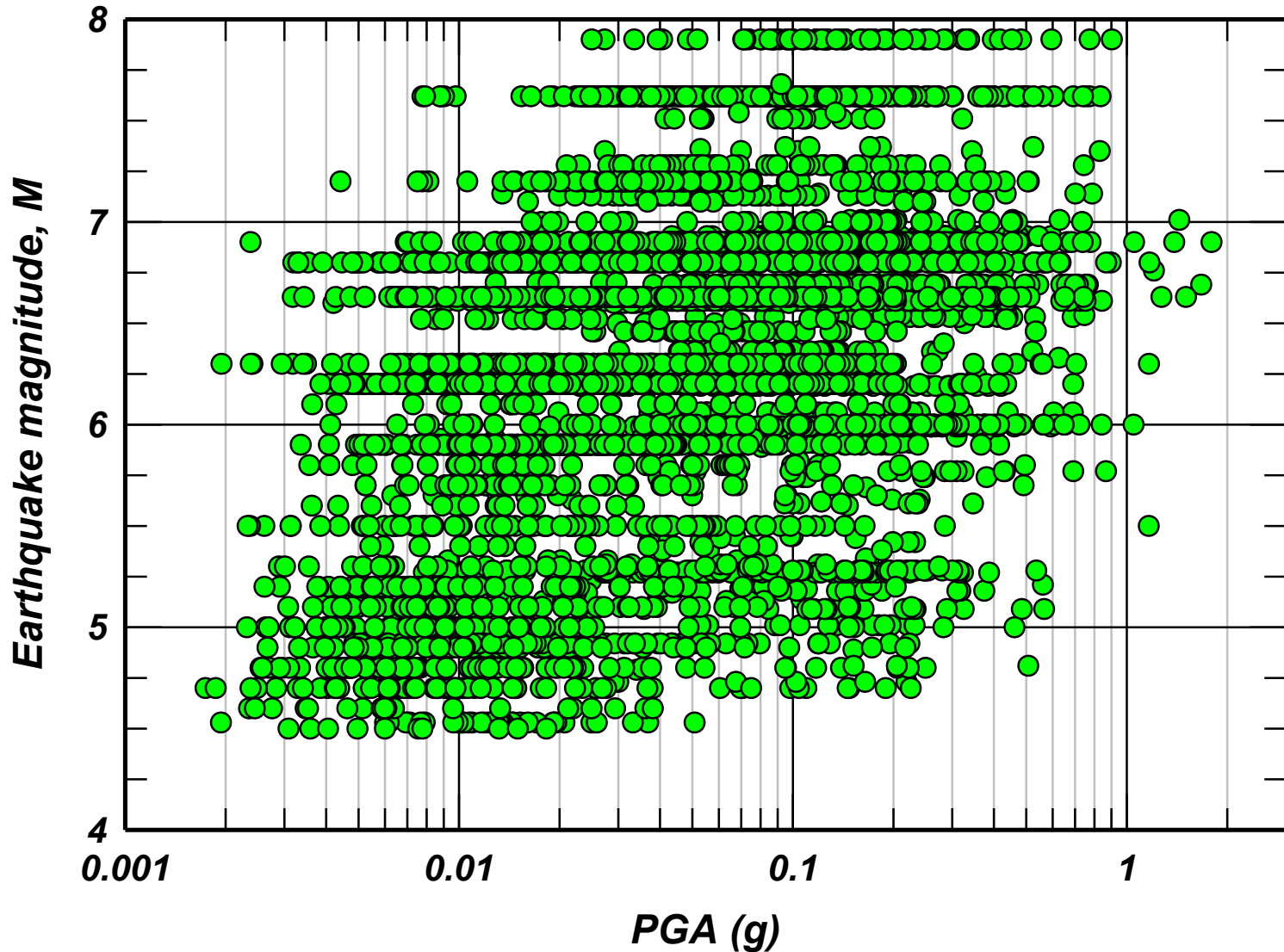
FF Records; Dist ≤ 160 km; $M \geq 4.5$



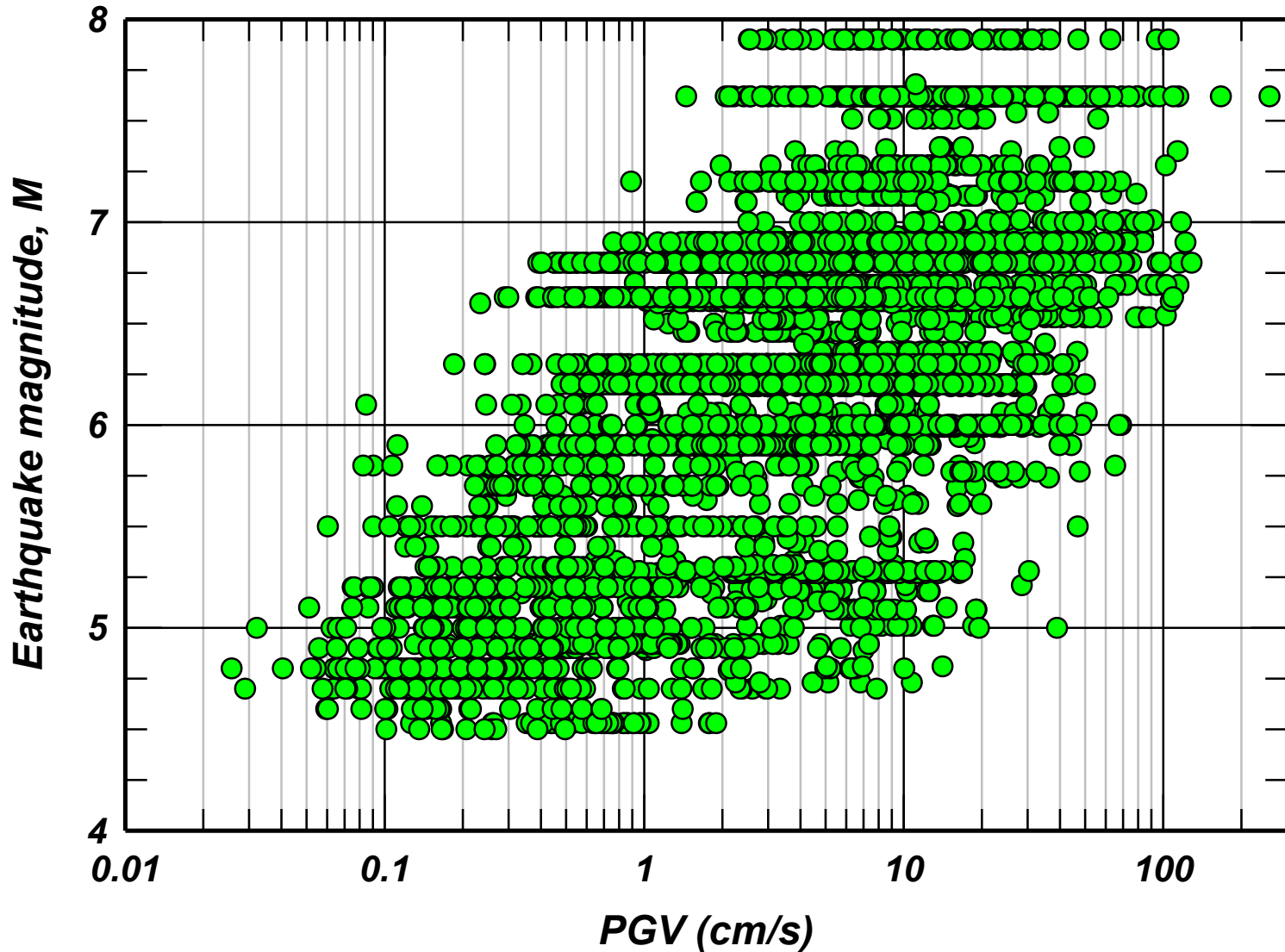
FF Records; Dist ≤ 160 km; $M \geq 4.5$



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FF Records; Dist ≤ 160 km; $M \geq 4.5$



DATA SET

Stations having $V_{s30} \geq 450$ m/s and $R \leq 160$ km

Total Number of records used = 1288

[147 recordings ($V_{s30} \geq 450$ m/s) from the Chi-Chi main shock were excluded]

$4.5 \leq M \leq 7.9$

$0.9 \text{ km} \leq R \leq 160 \text{ km}$

$450 \text{ m/s} \leq V_{s30} \leq 2016 \text{ m/s}$

[only 10 recordings at site with $V_{s30} > 1200$ m/s]

$$\ln(y) = (a_1 + a_2 M) - (b_1 + b_2 M) \ln(R + 10) + gR + x(V_{s30} - 450) + f F$$

	Period (sec)	α_1	α_2	β_1	β_2	γ	ϕ	ξ
M > 6.75	0.01 (PGA)	5.5107	-0.3530	2.9832	-0.2339	-0.00125	0.12	-0.00033
	Period (sec)	α_1	α_2	β_1	β_2	γ	ϕ	ξ
M ≤ 6.75	0.01 (PGA)	3.5858	-0.0678	2.9832	-0.2339	-0.00125	0.12	-0.00033

Range of M ==>

4.5 to 8

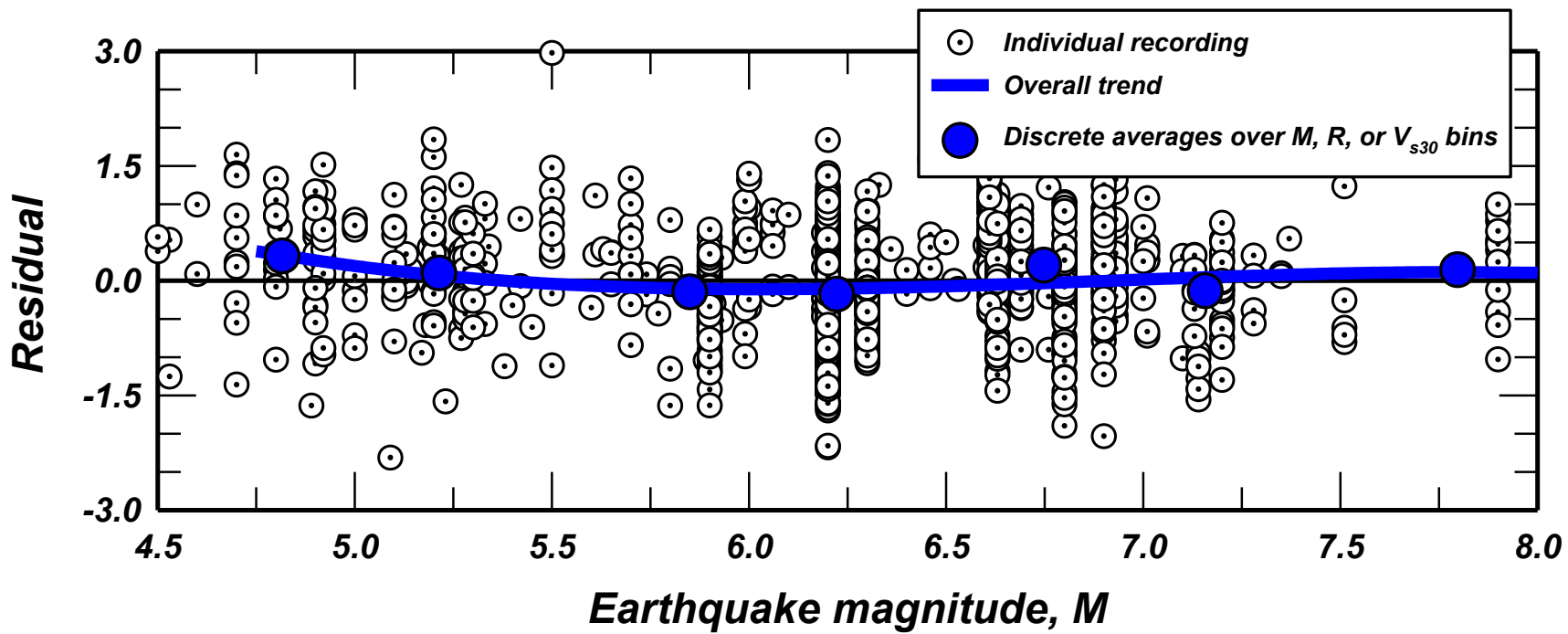
Range of R ==>

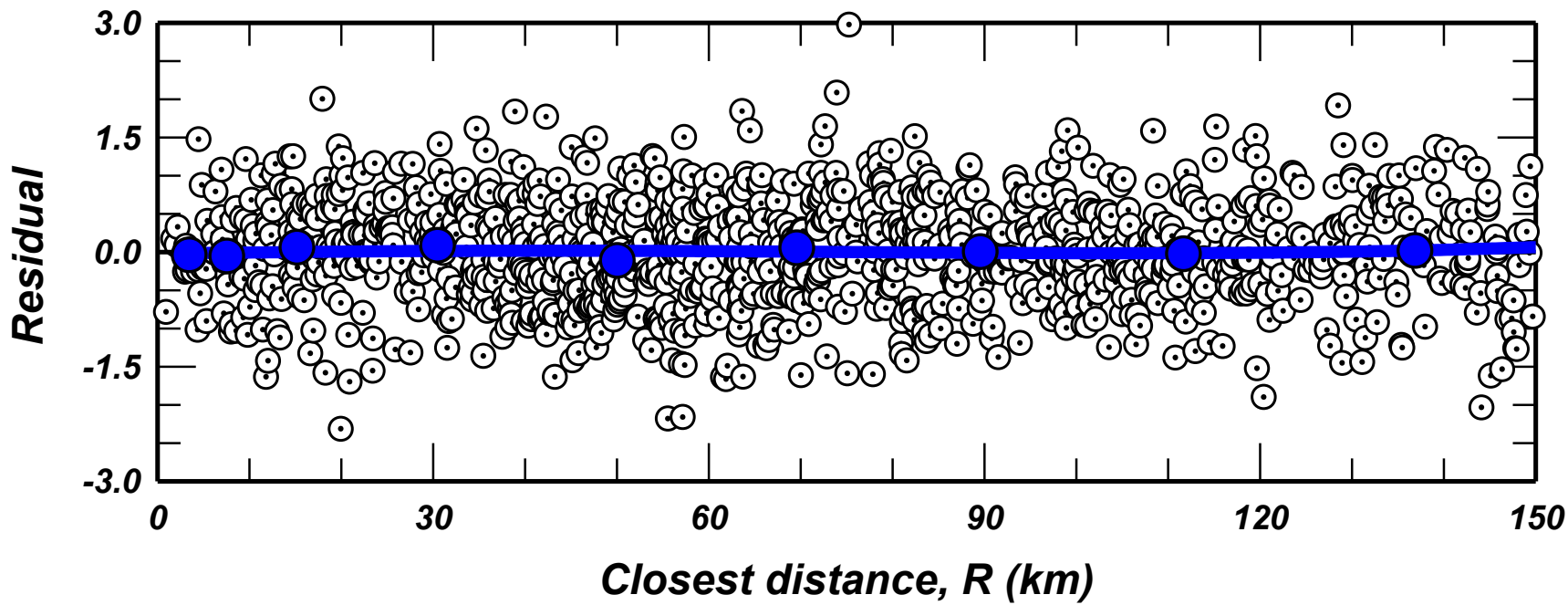
0 to 160 km

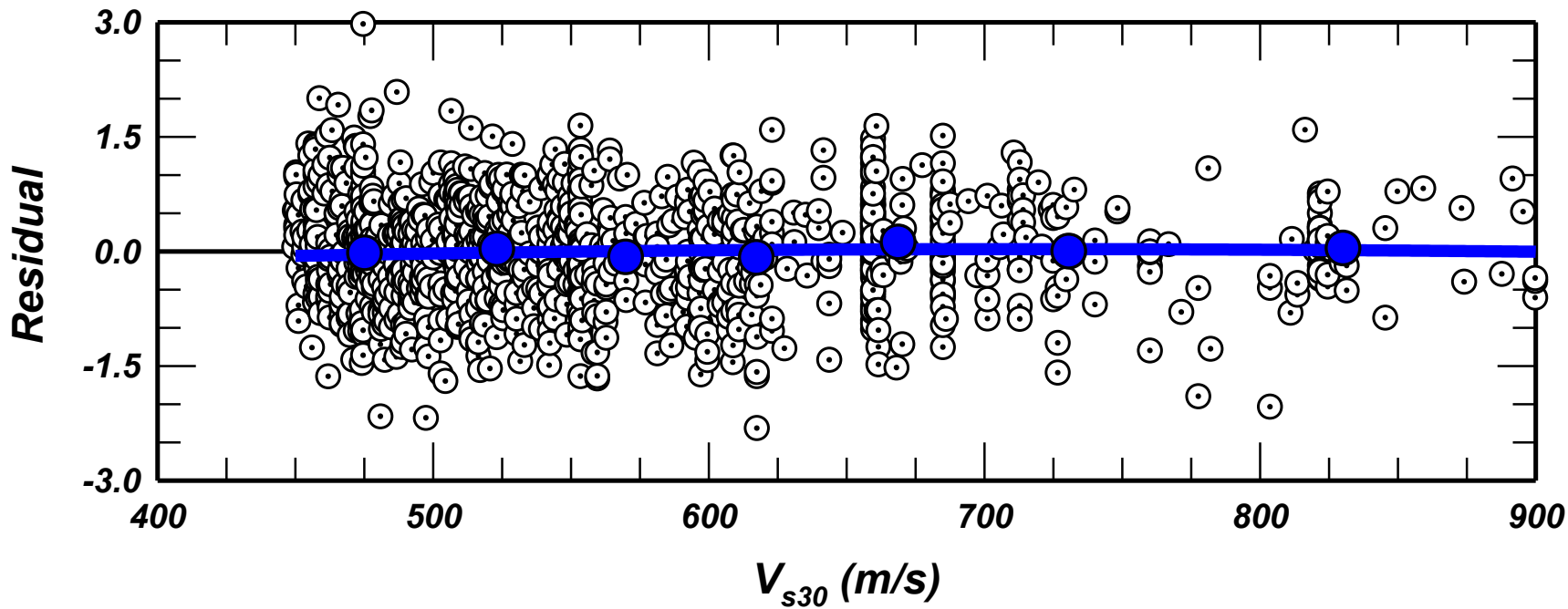
Range of Vs30 ==>

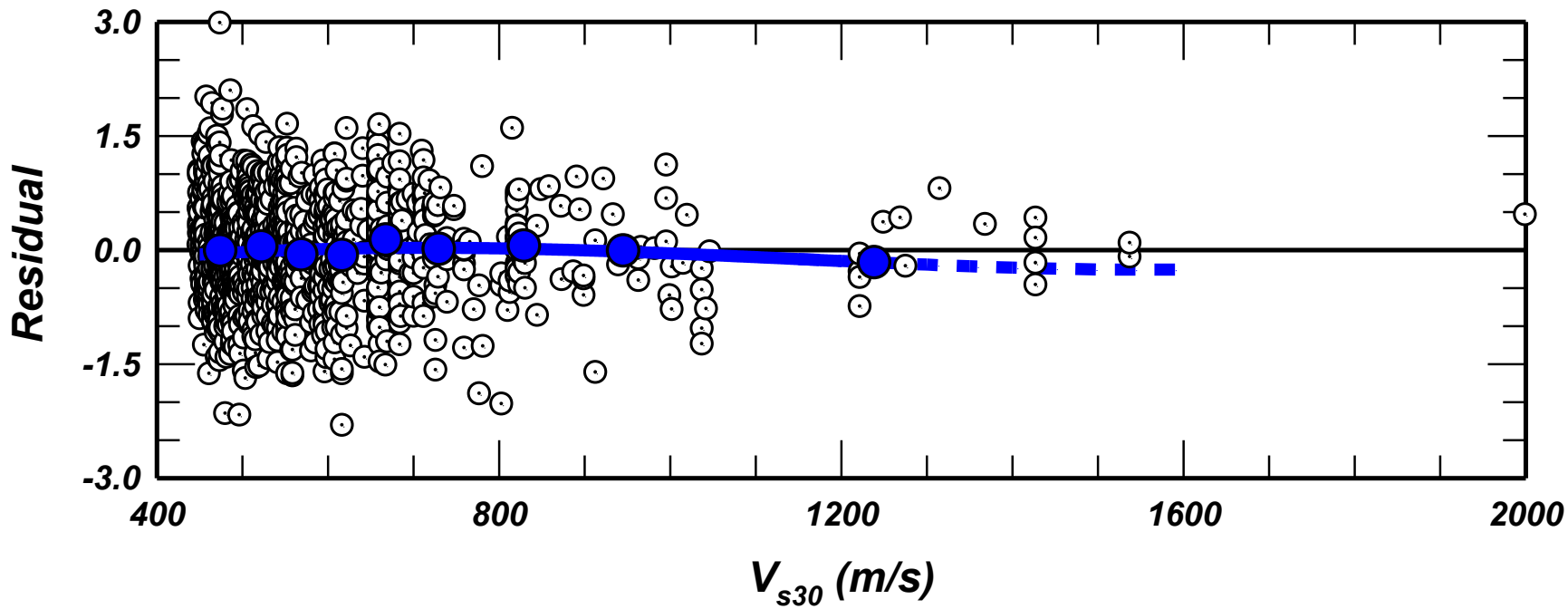
450 ≤ to ≤ 2100 m/s

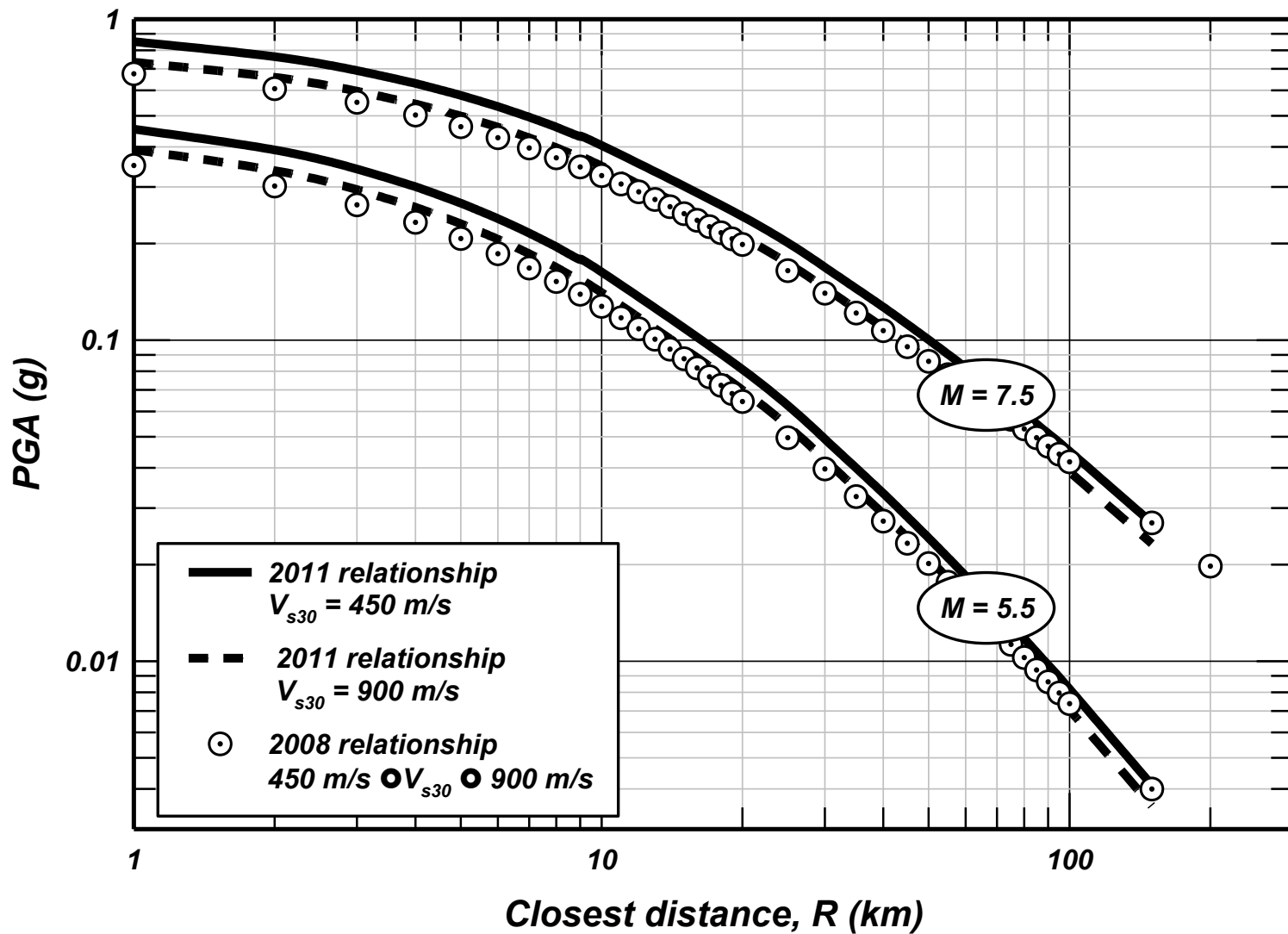
IMI_2011

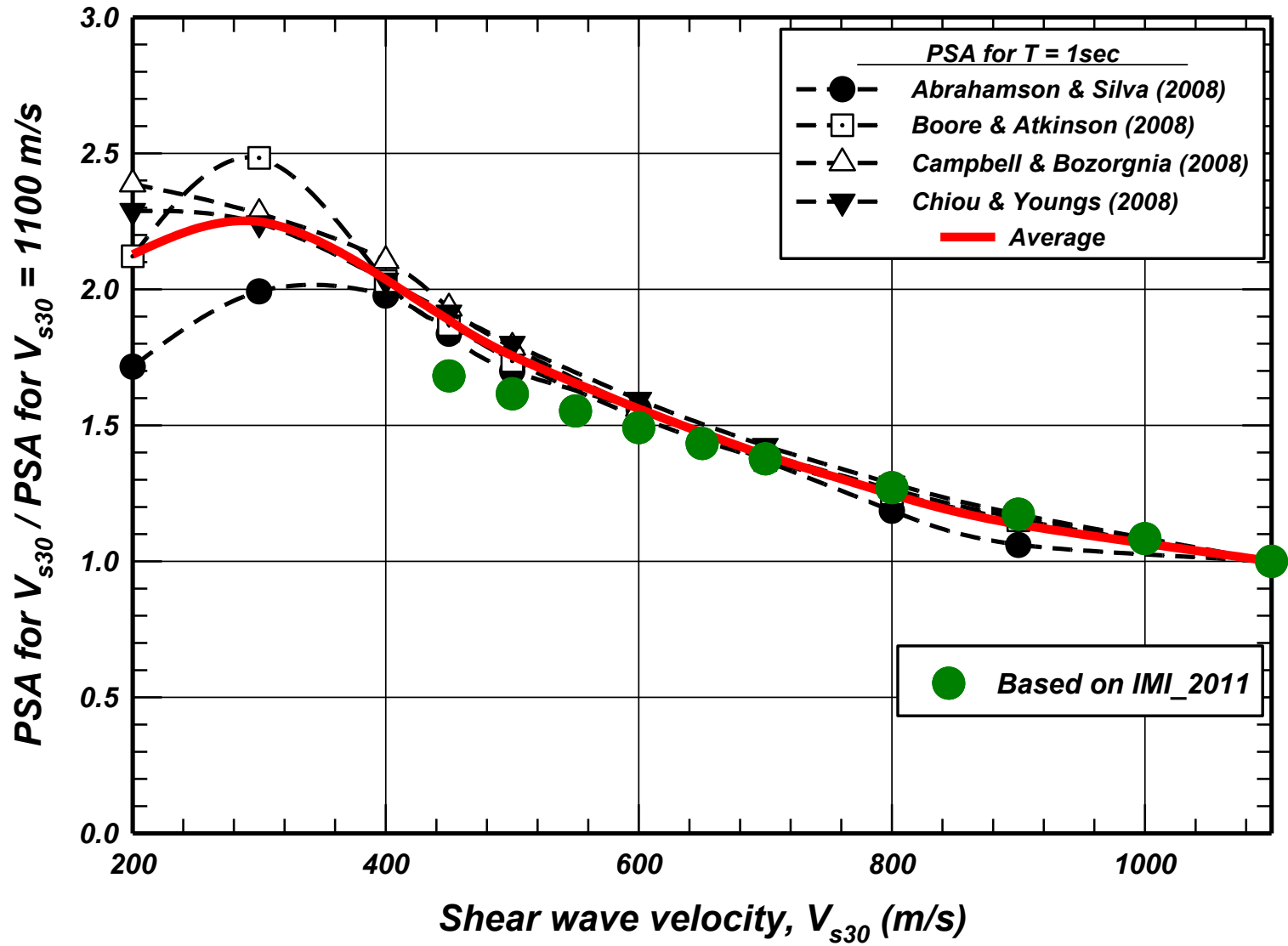












***WHAT DO THE NGA
DATA SHOW?***

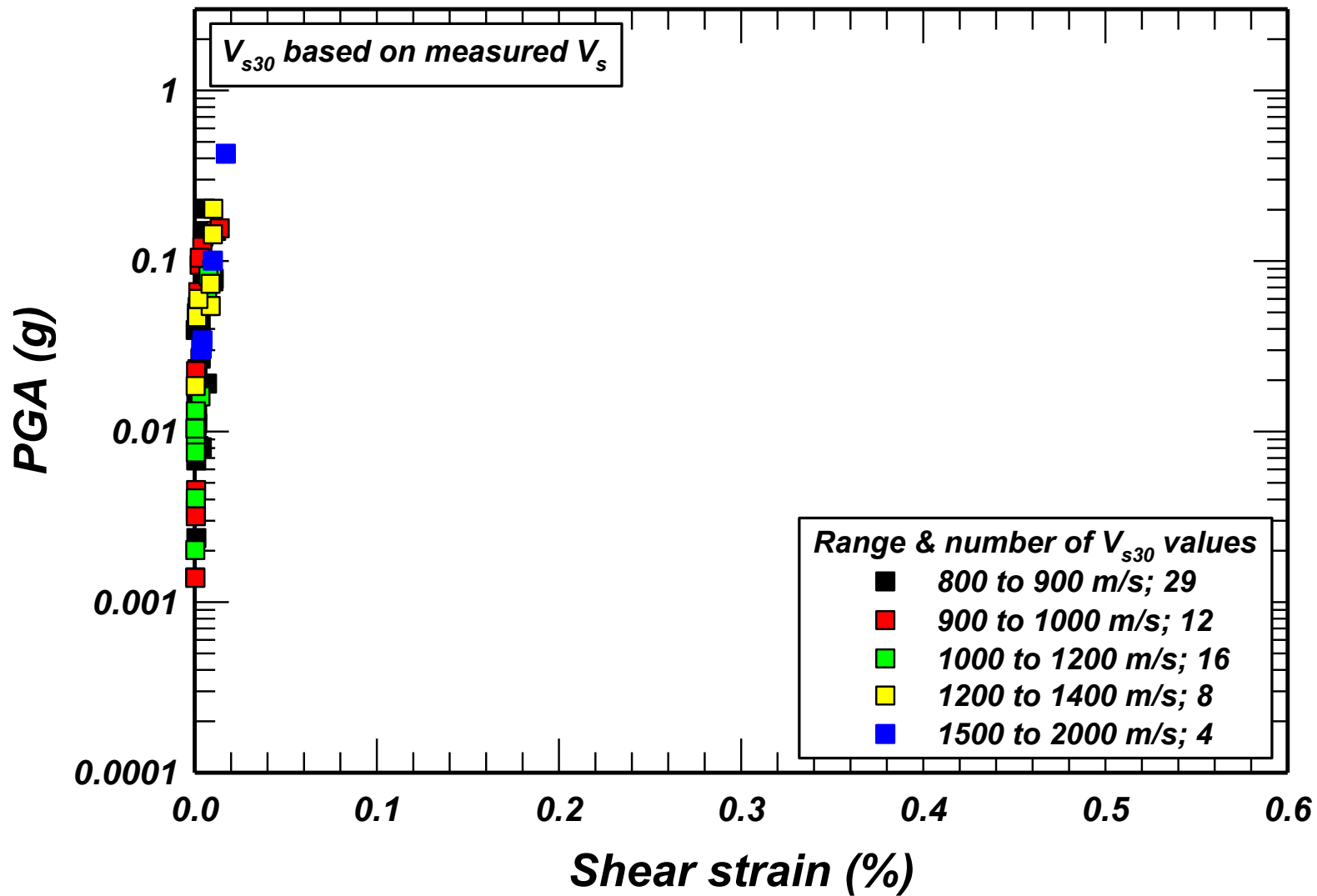


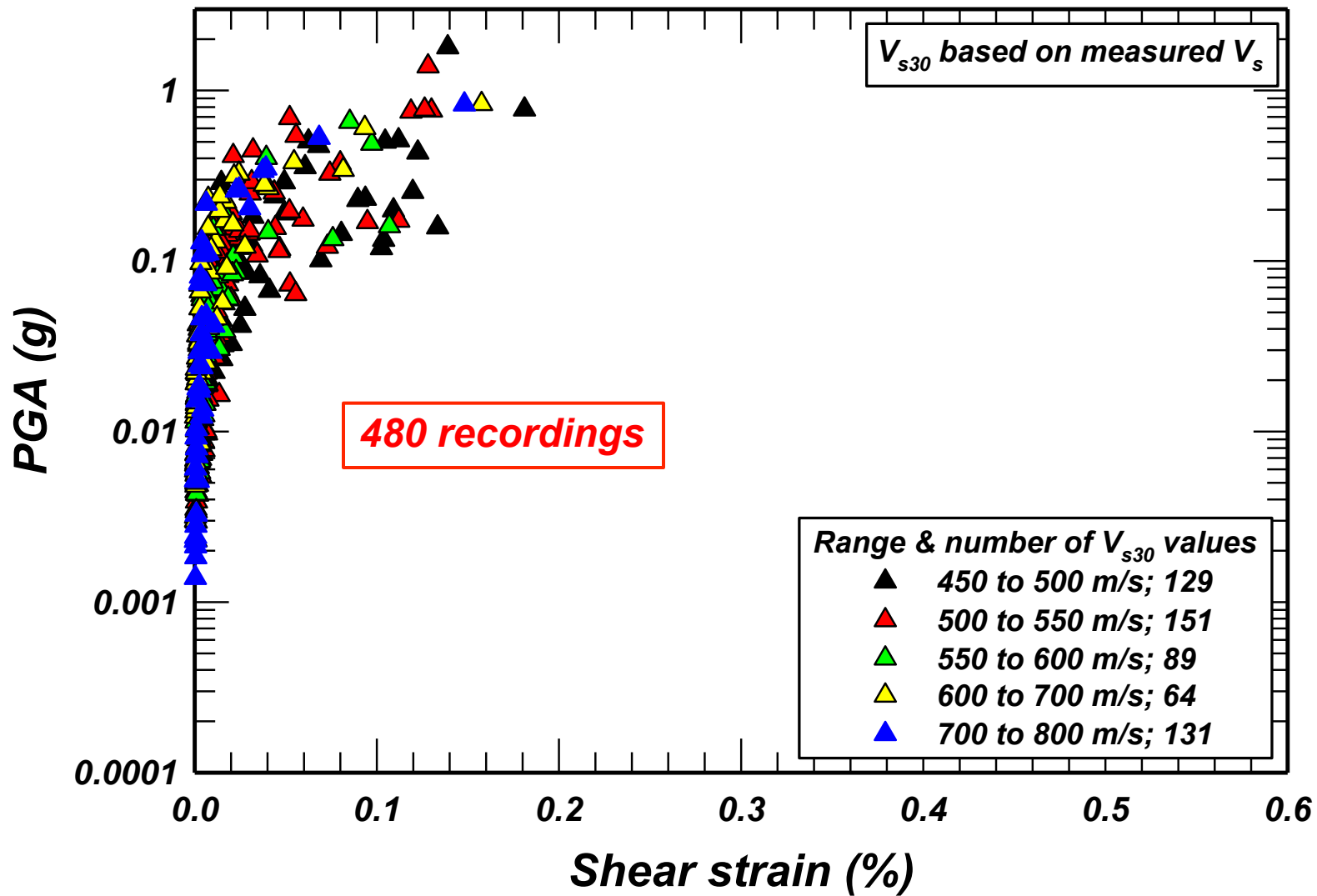
Examination in terms of the ratio of:

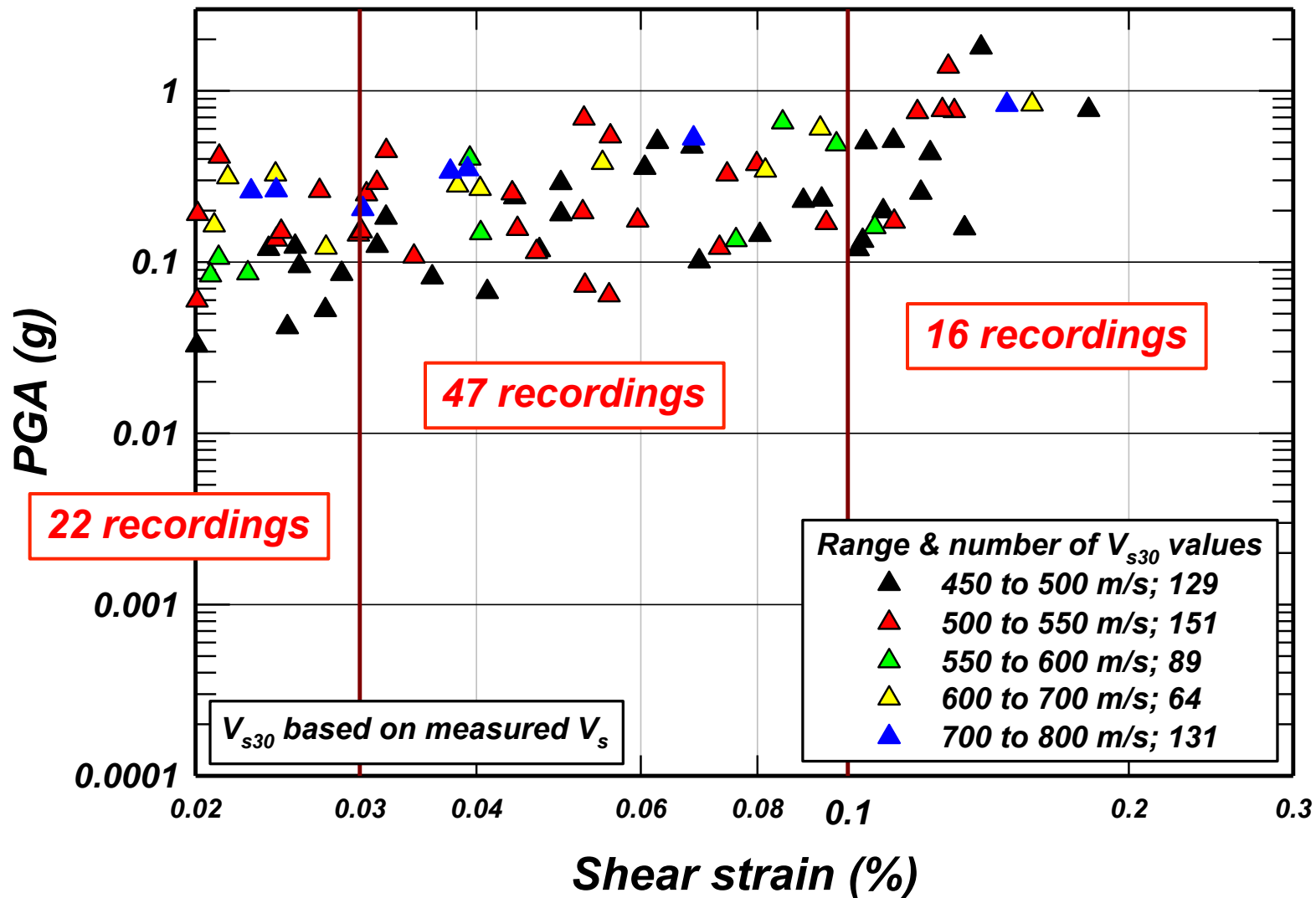
$$***PGV/V_{s30}***$$

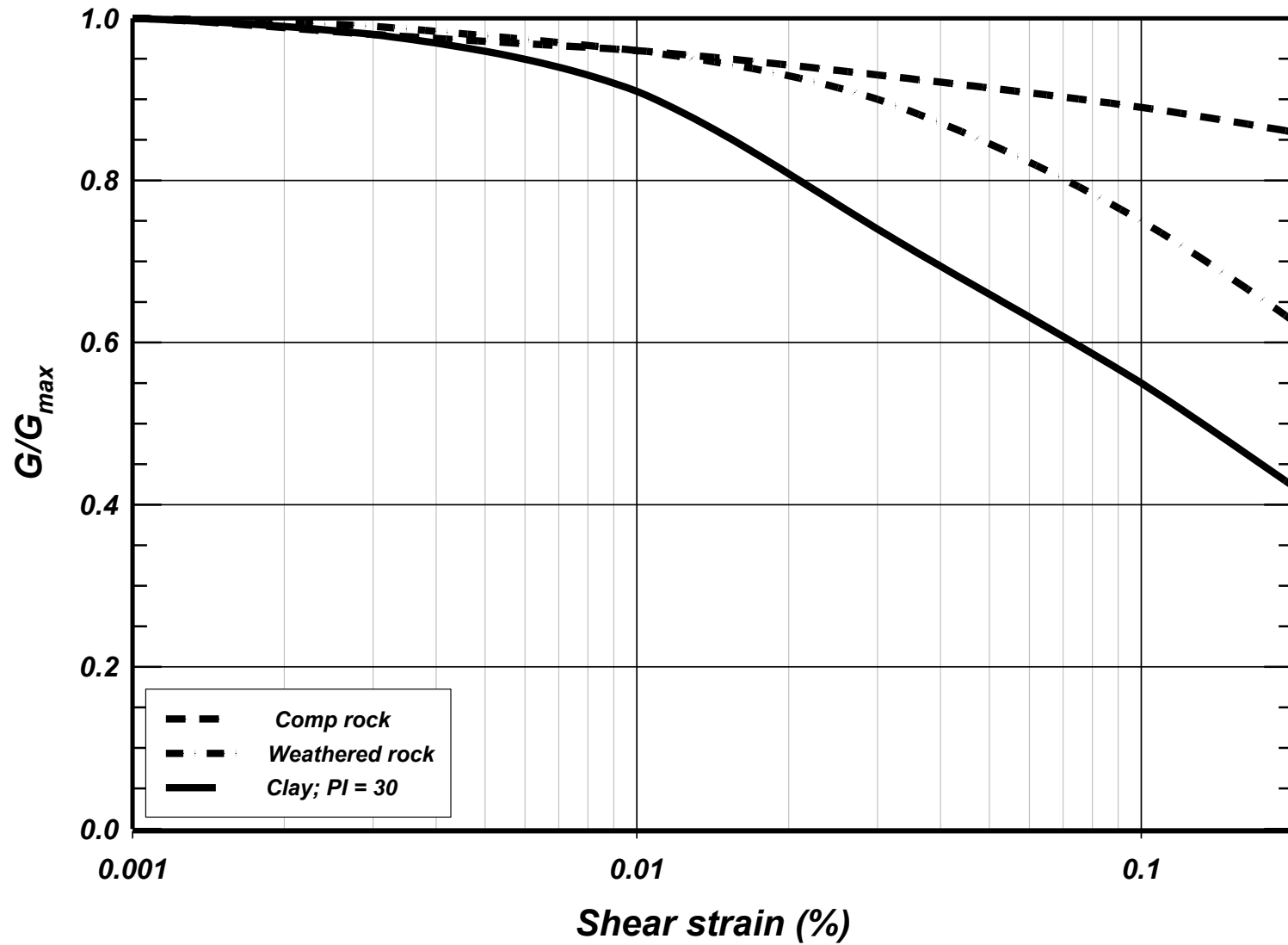
which may be considered as a "proxy" for shear strain induced by the earthquake ground motions

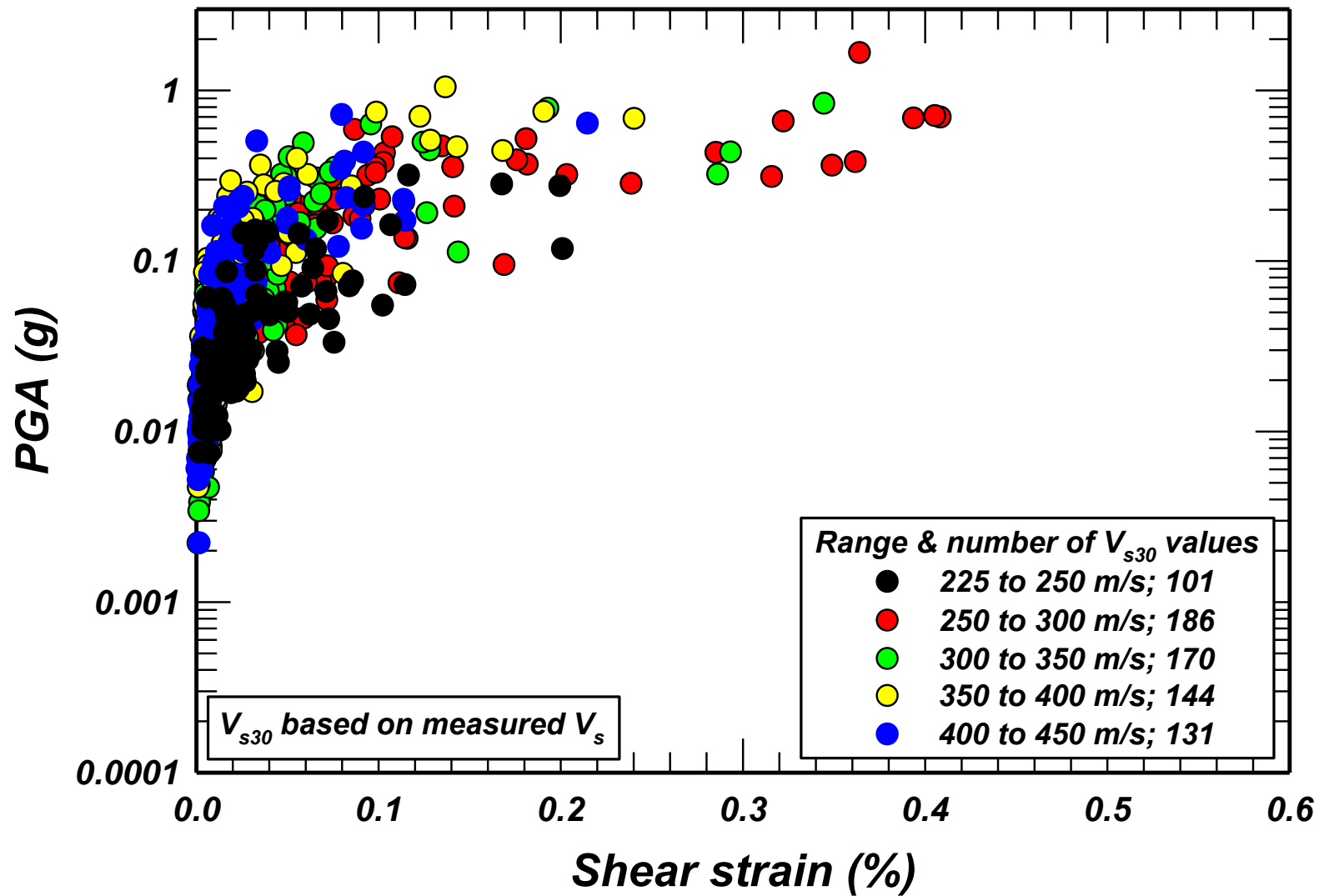
Plotting PGA versus this ratio can then be examined as if it were a "stress- strain" relationship

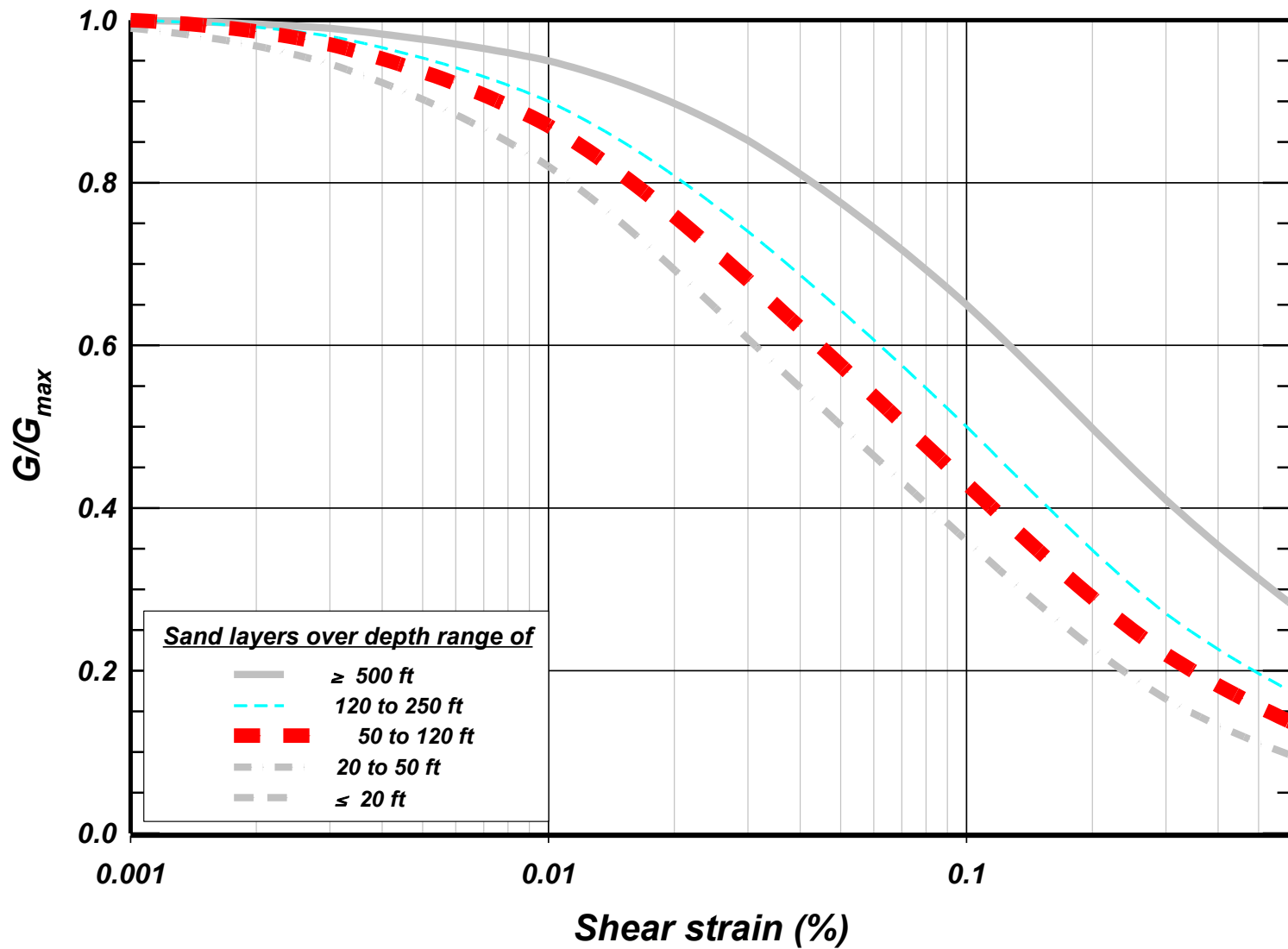


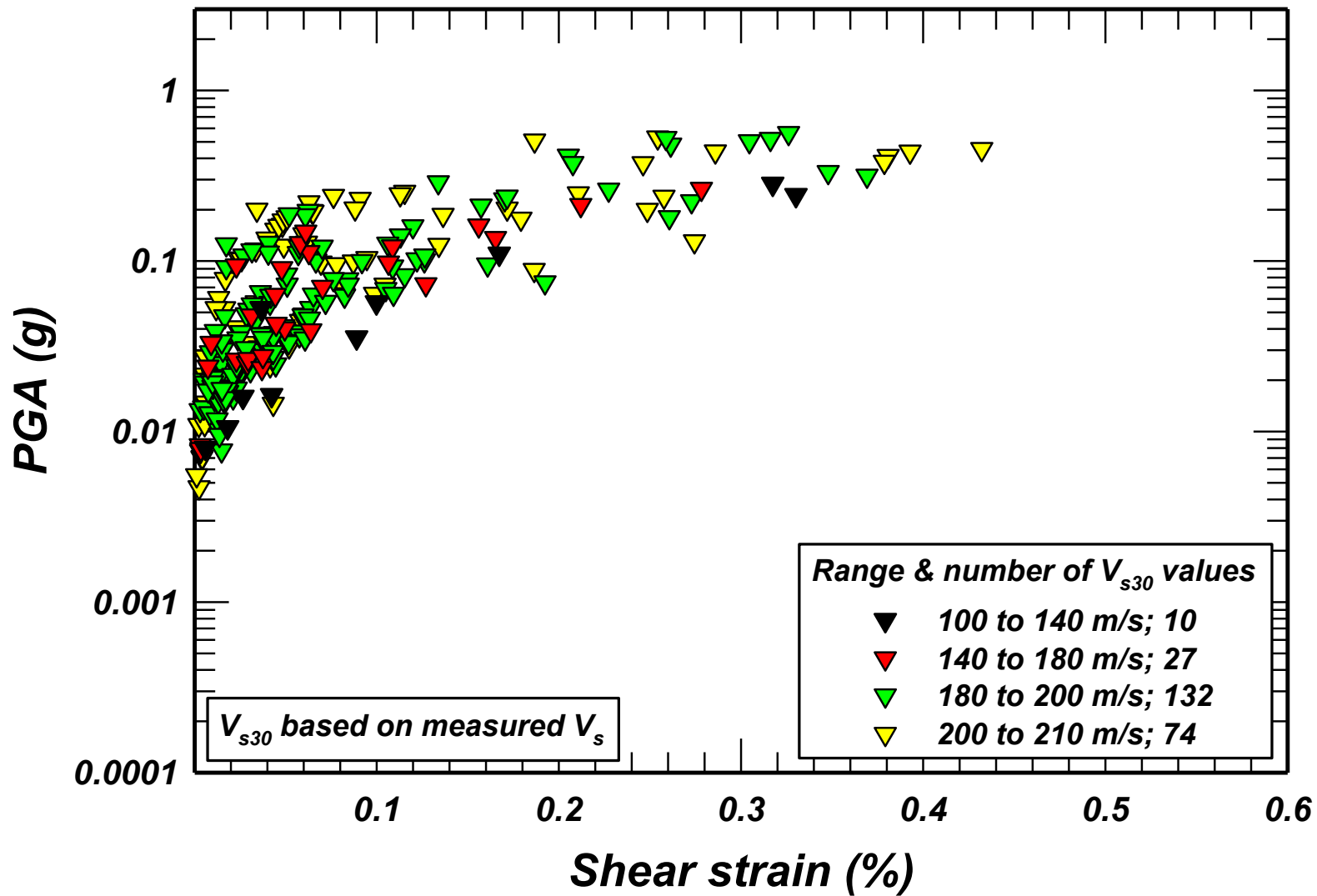












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University of Missouri-Rolla

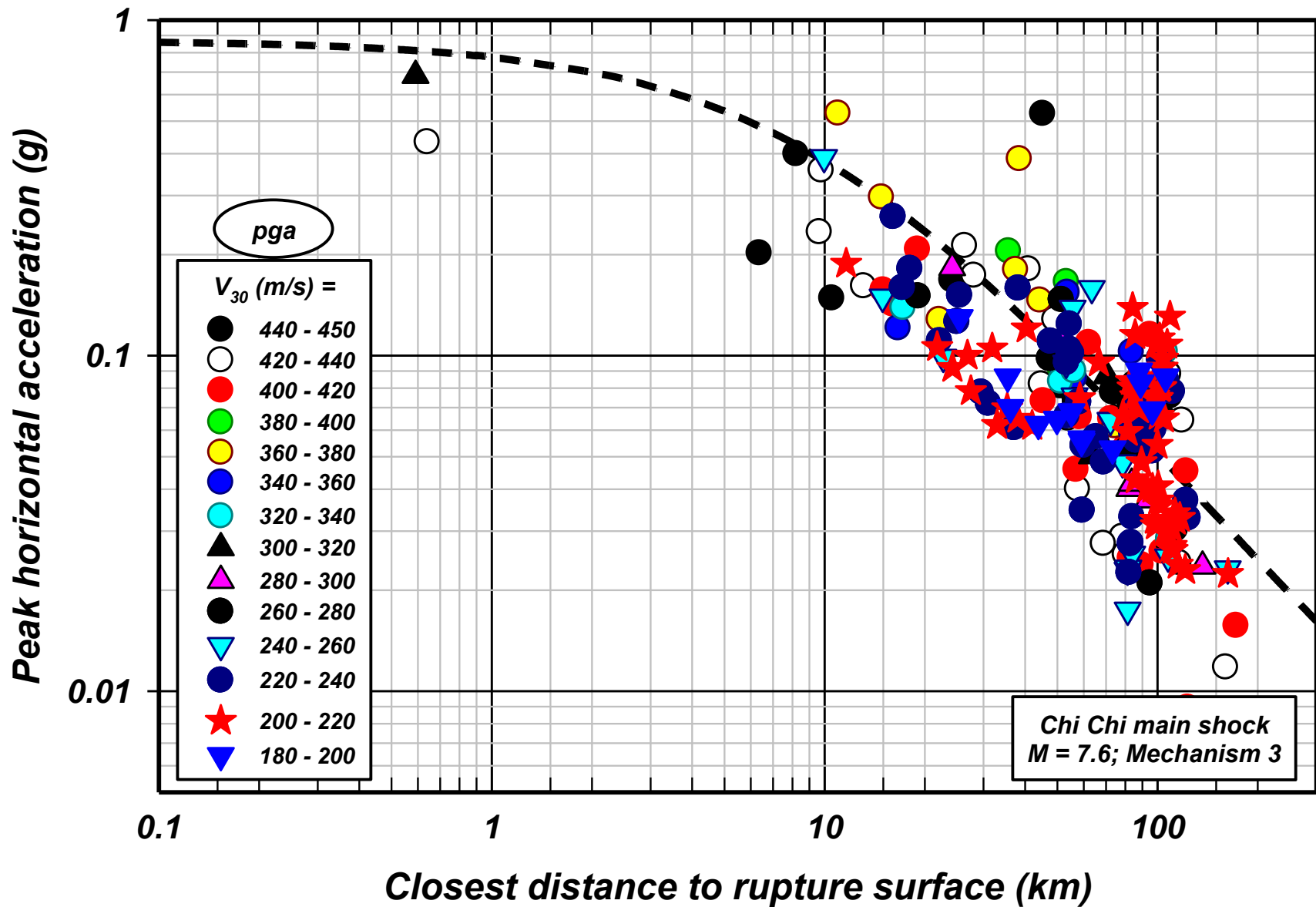
Rolla, Missouri

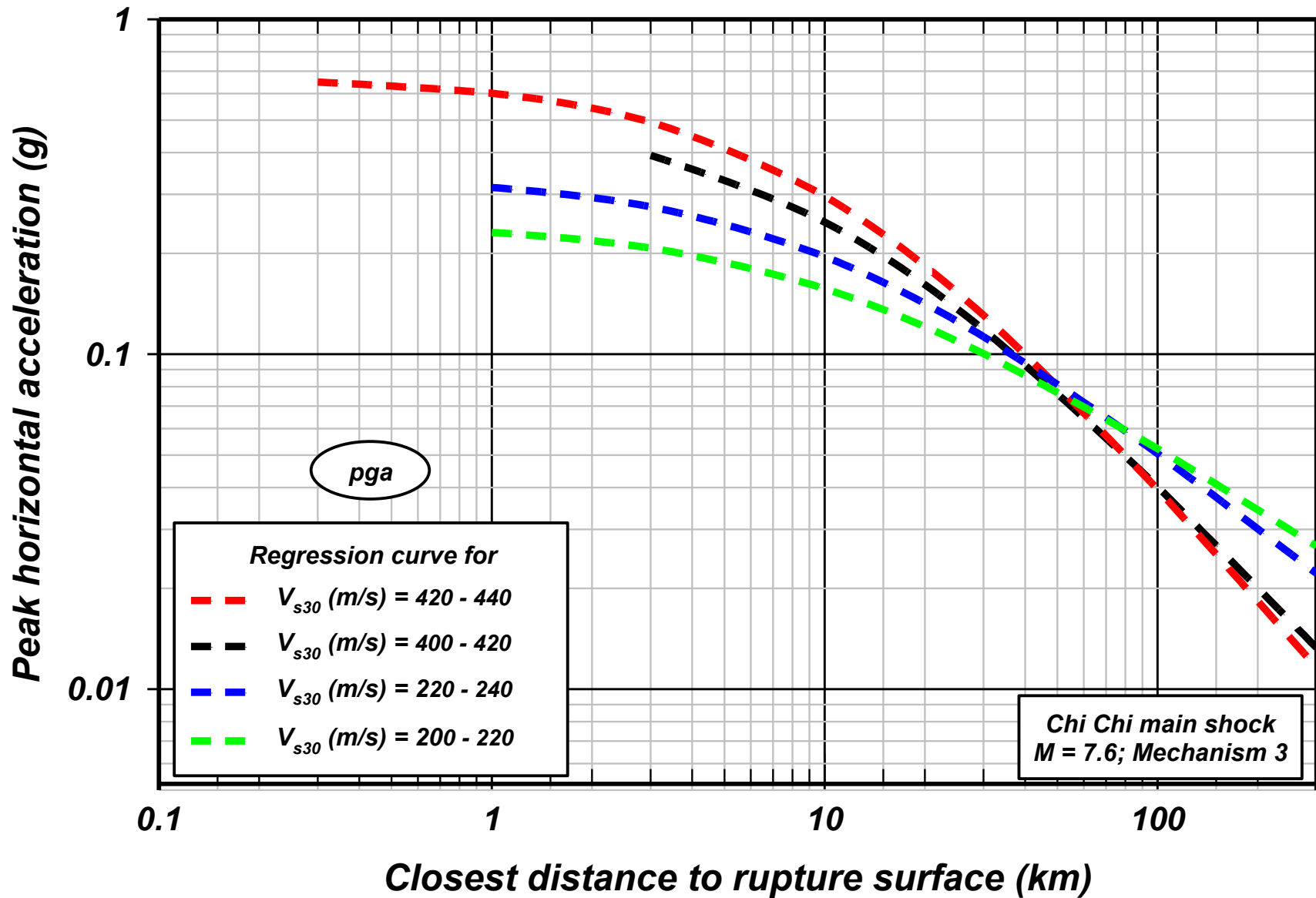
Examination in terms of :

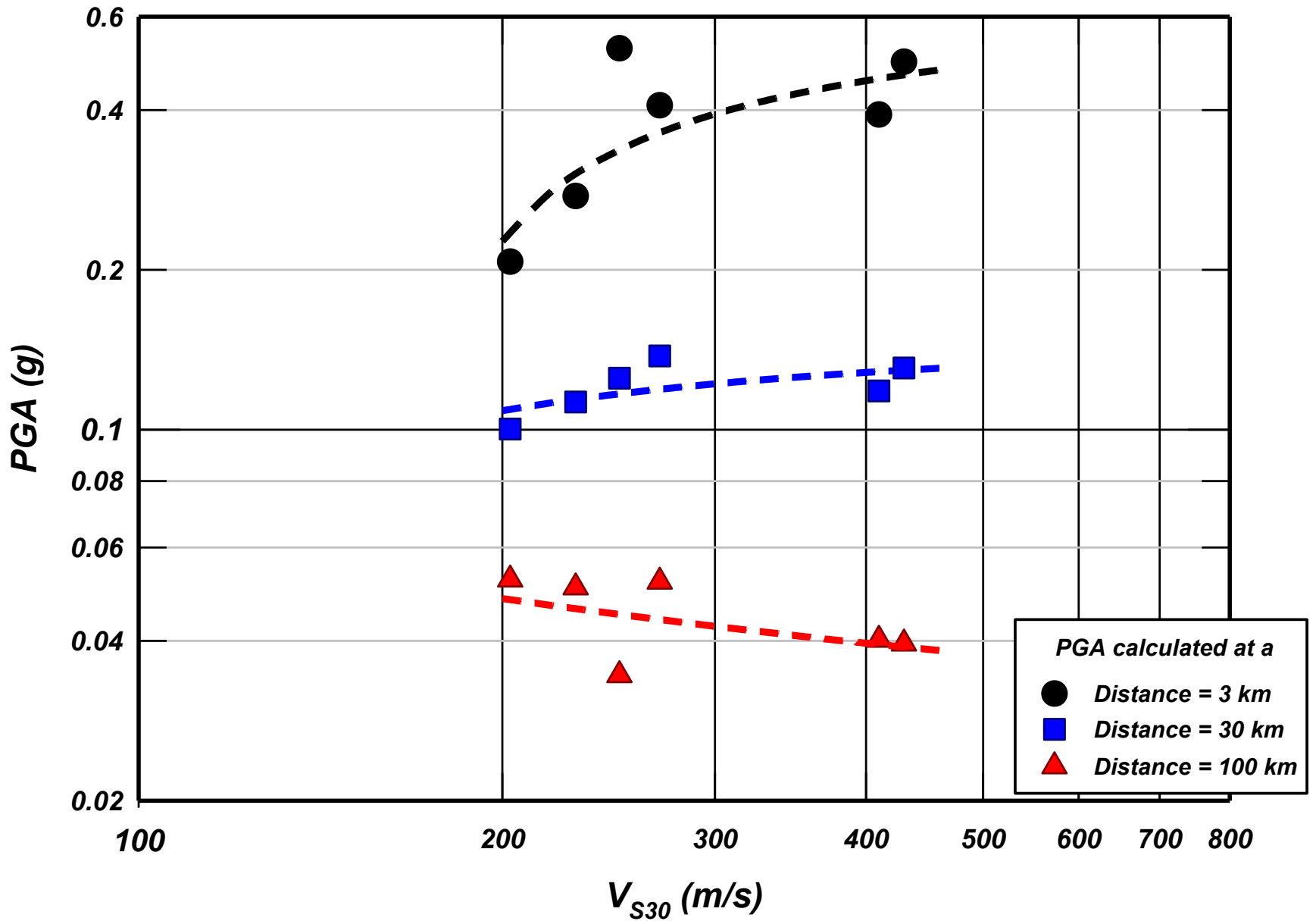
***Variations of PGA and PSA, at $T = 1$ sec,
with Distance***

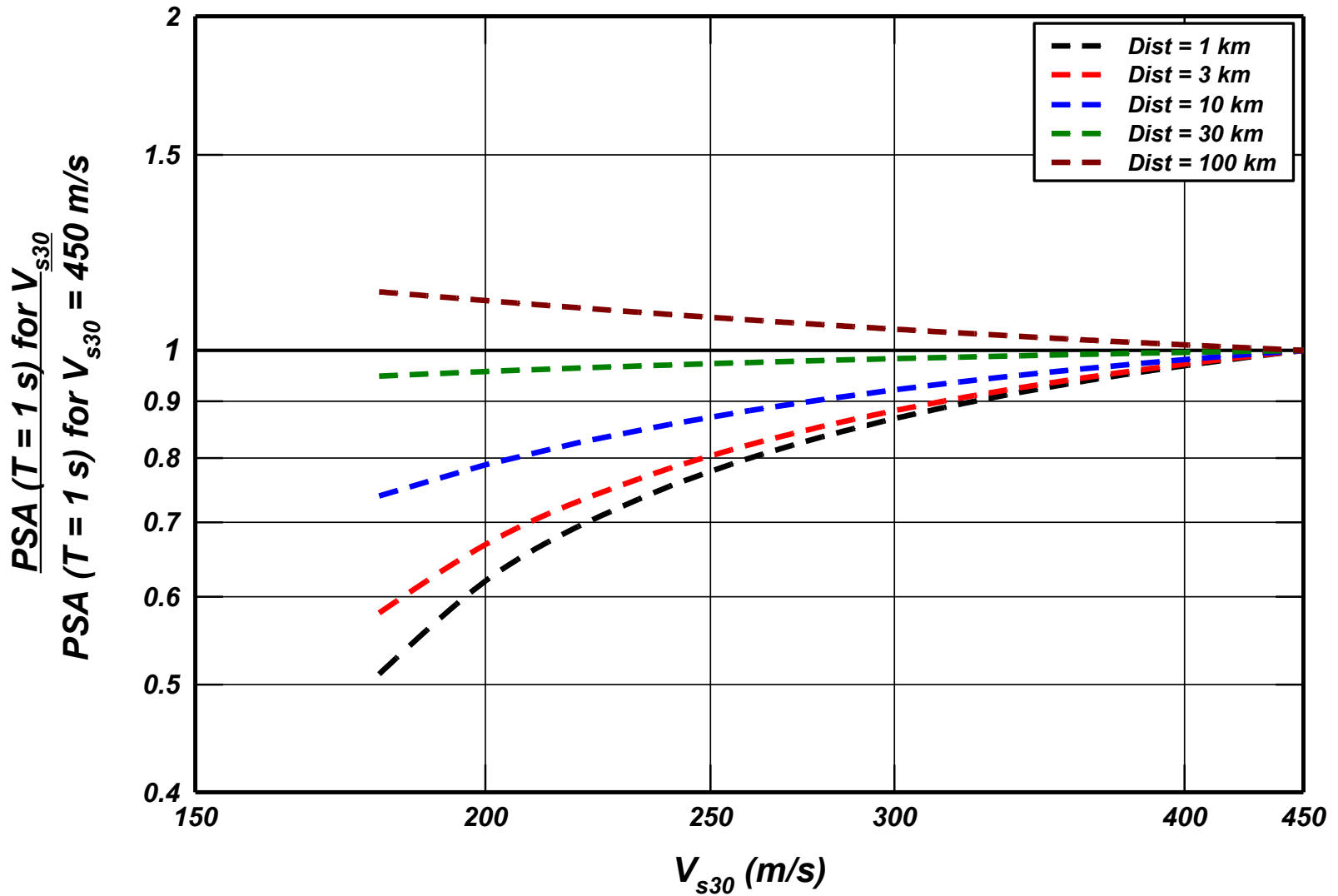
For various bins of V_{s30}

Chi-Chi main shock data



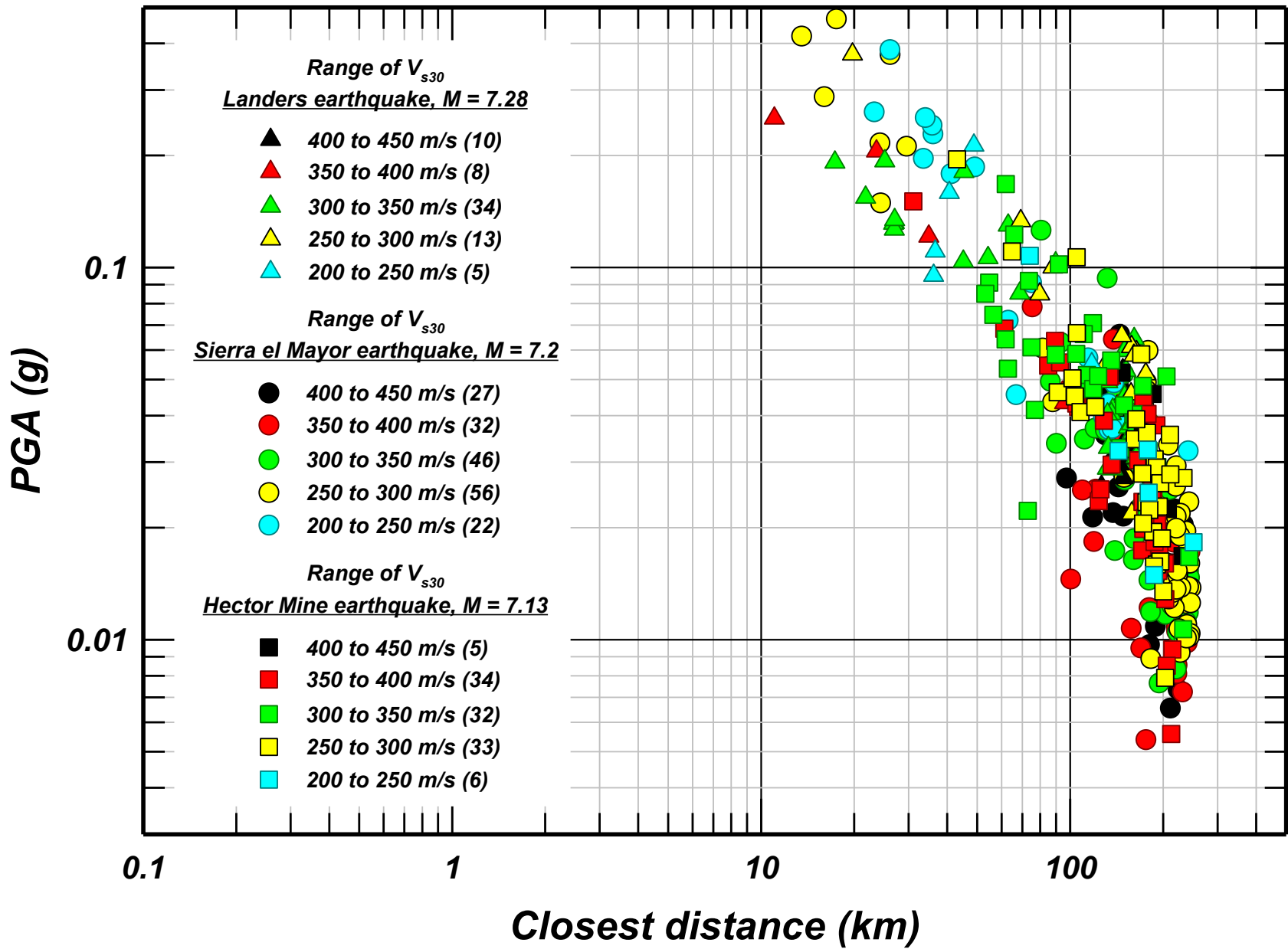


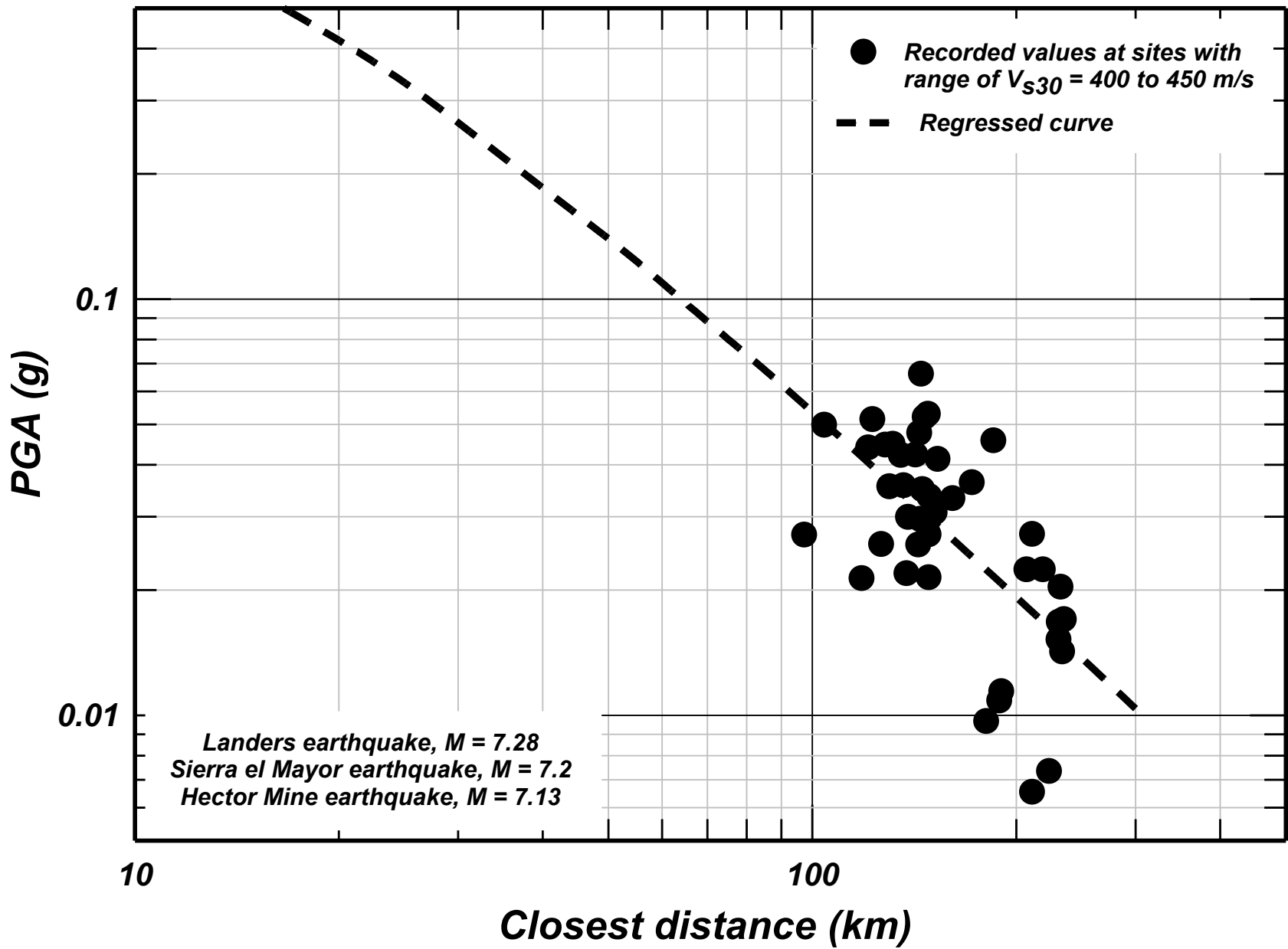


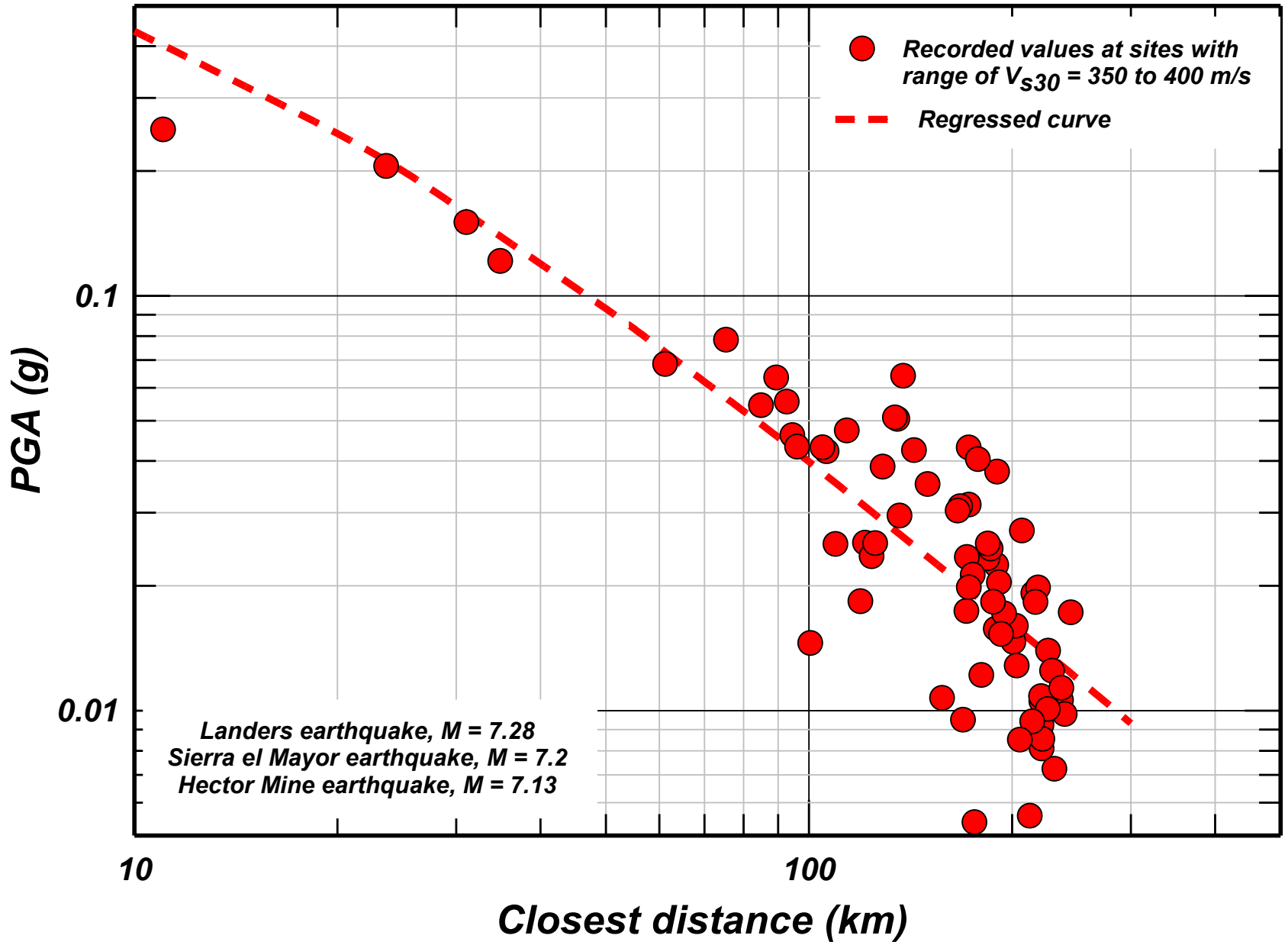


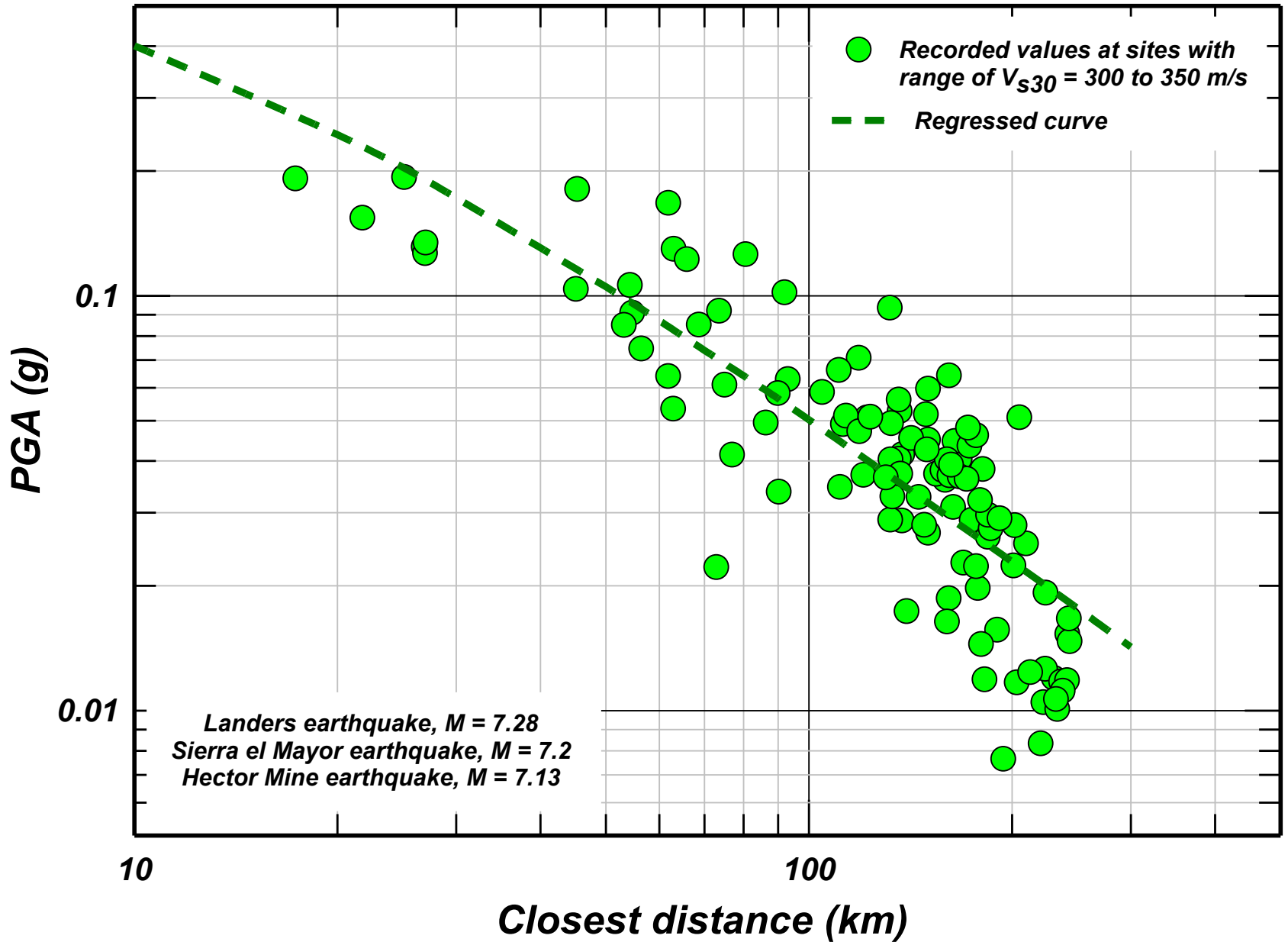
Based on Chi-Chi Recordings

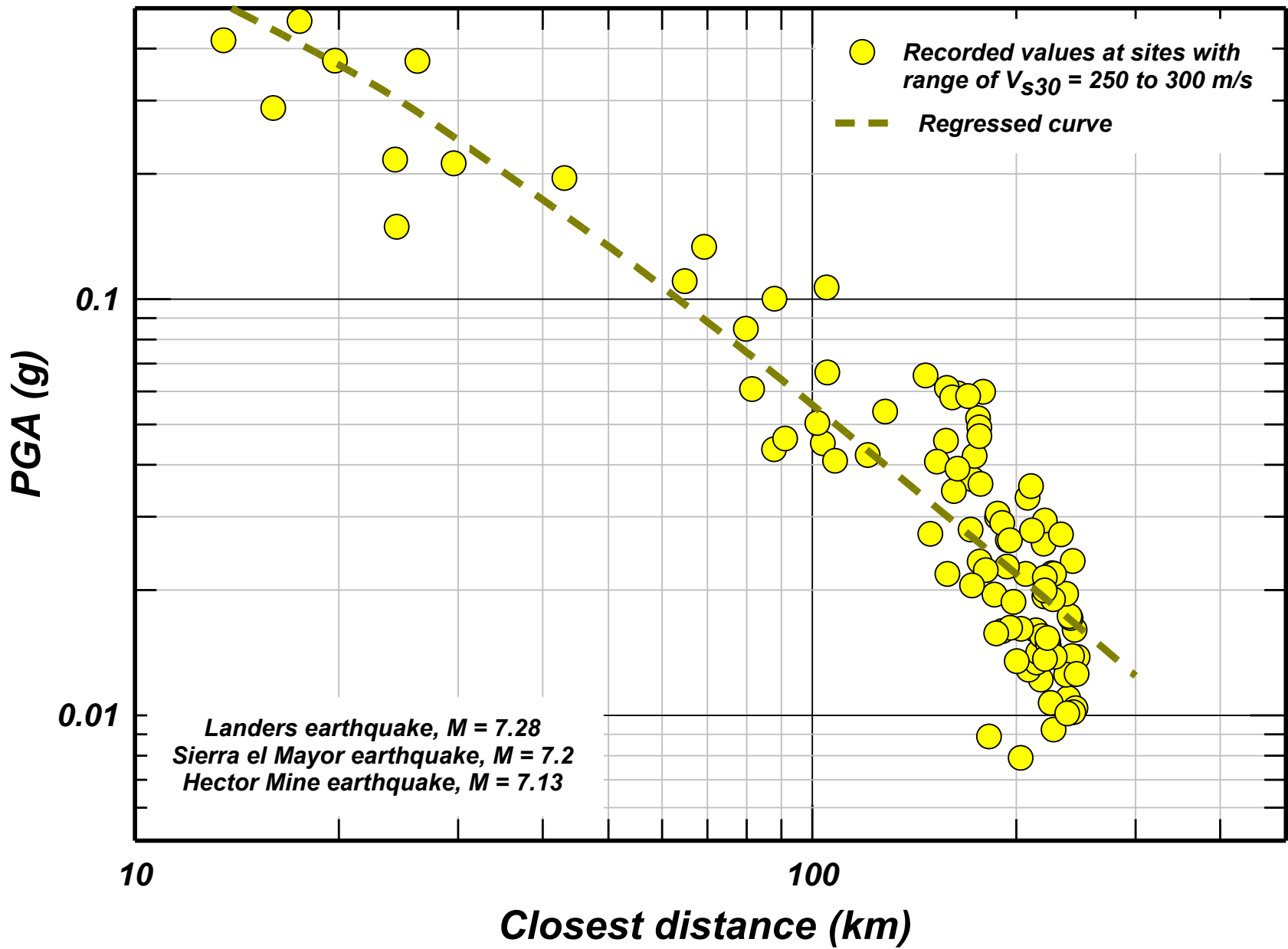
***Based on recorded data from
other than the Chi-Chi earthquake***

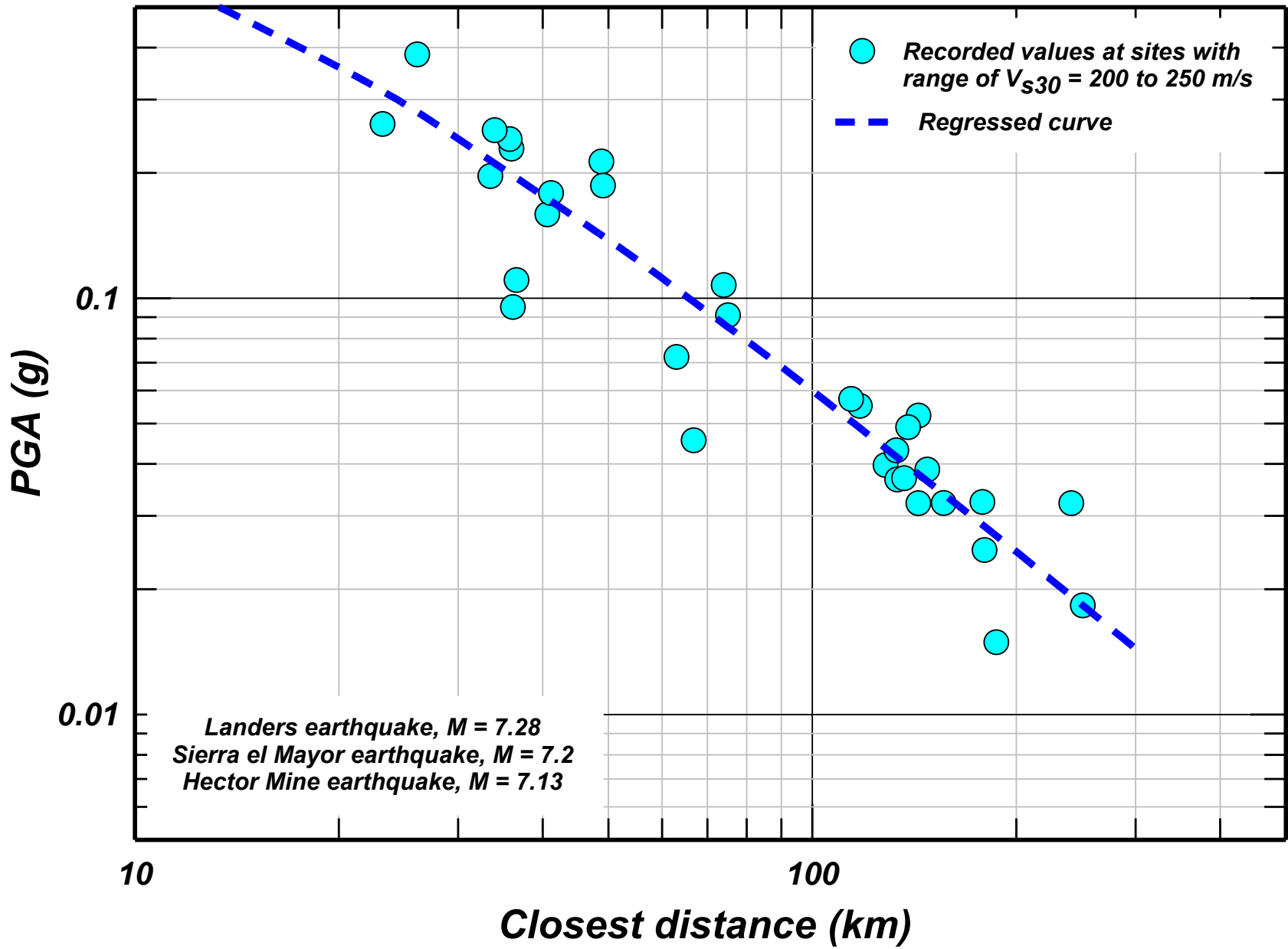


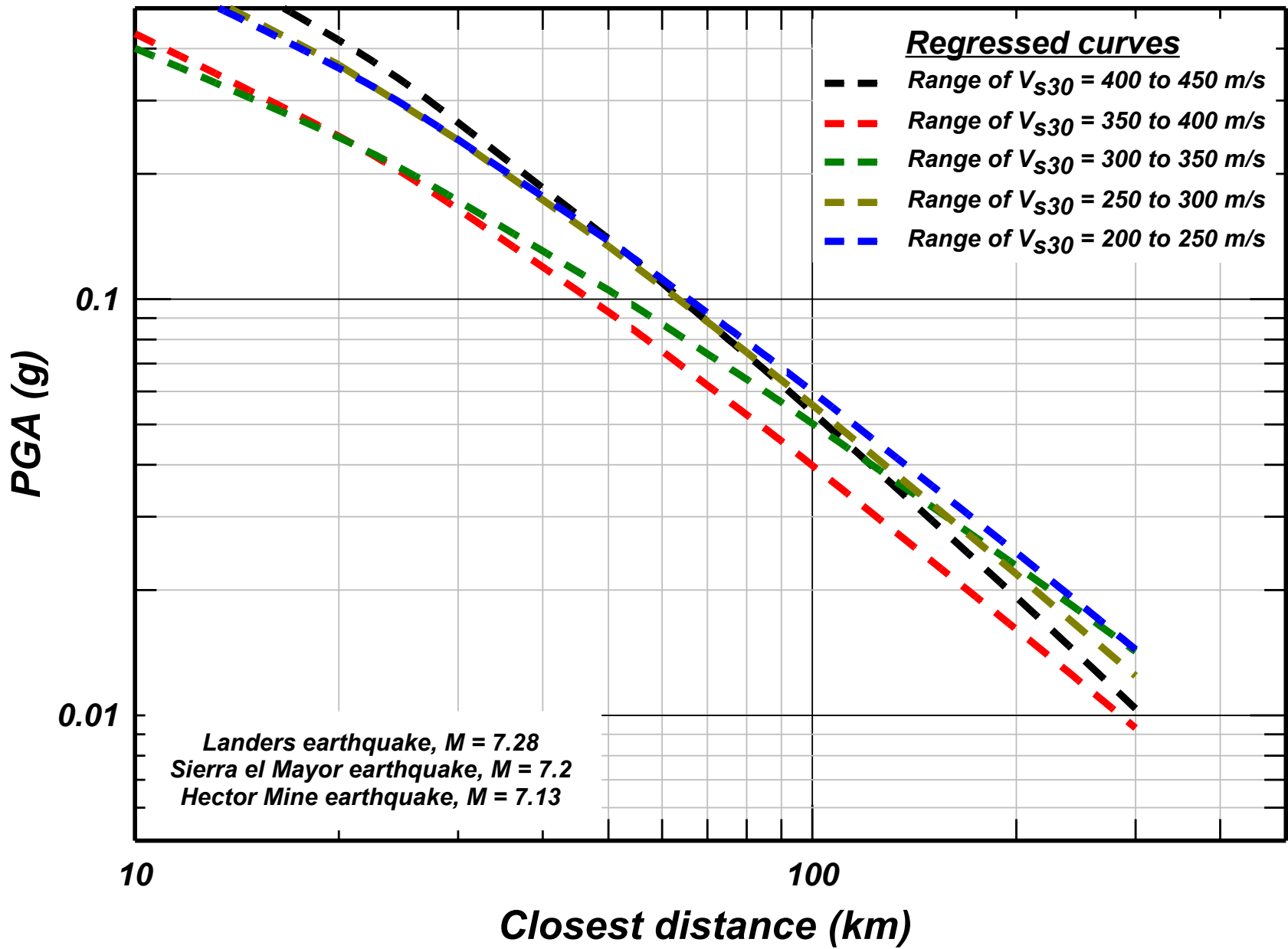


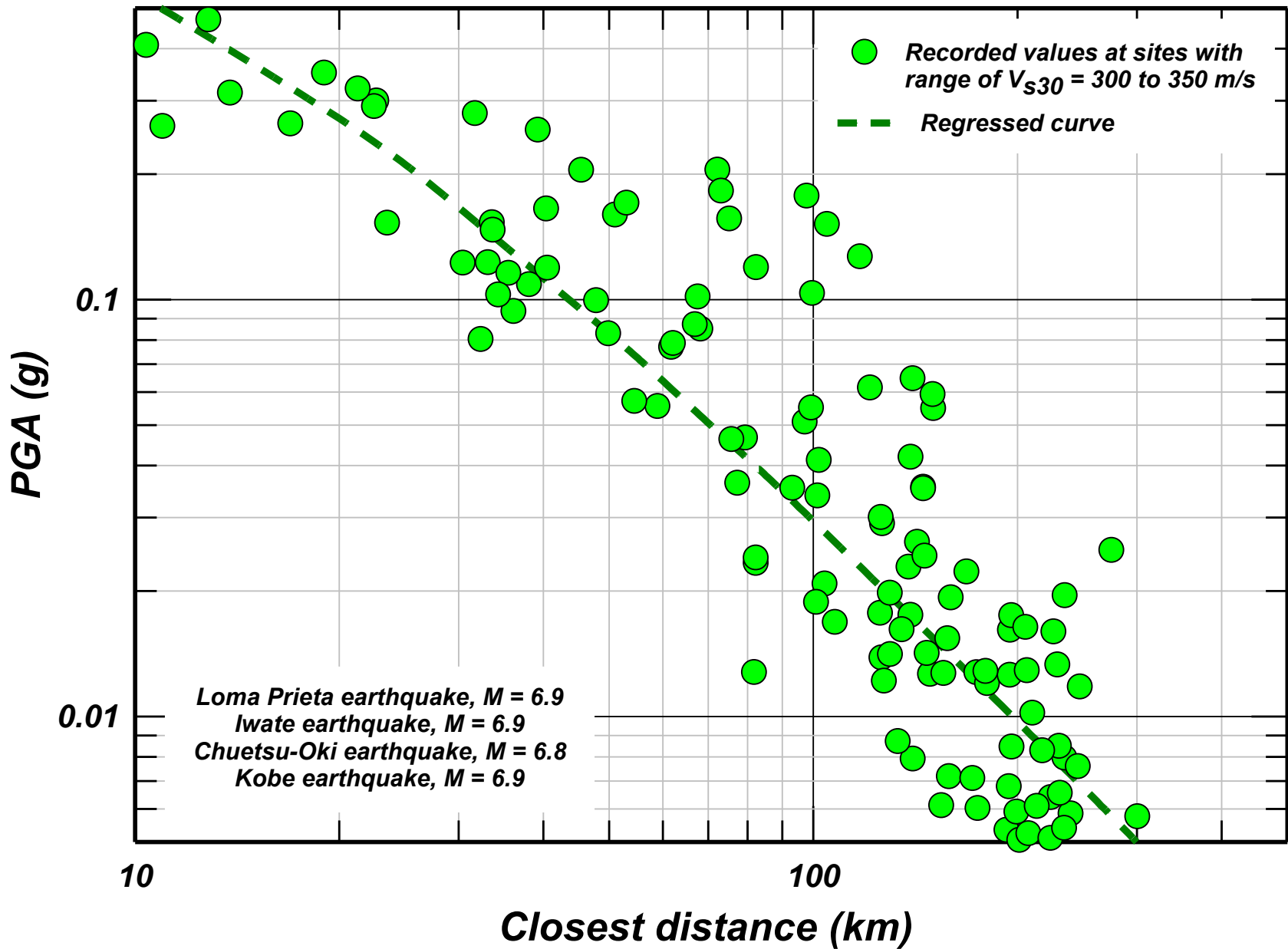


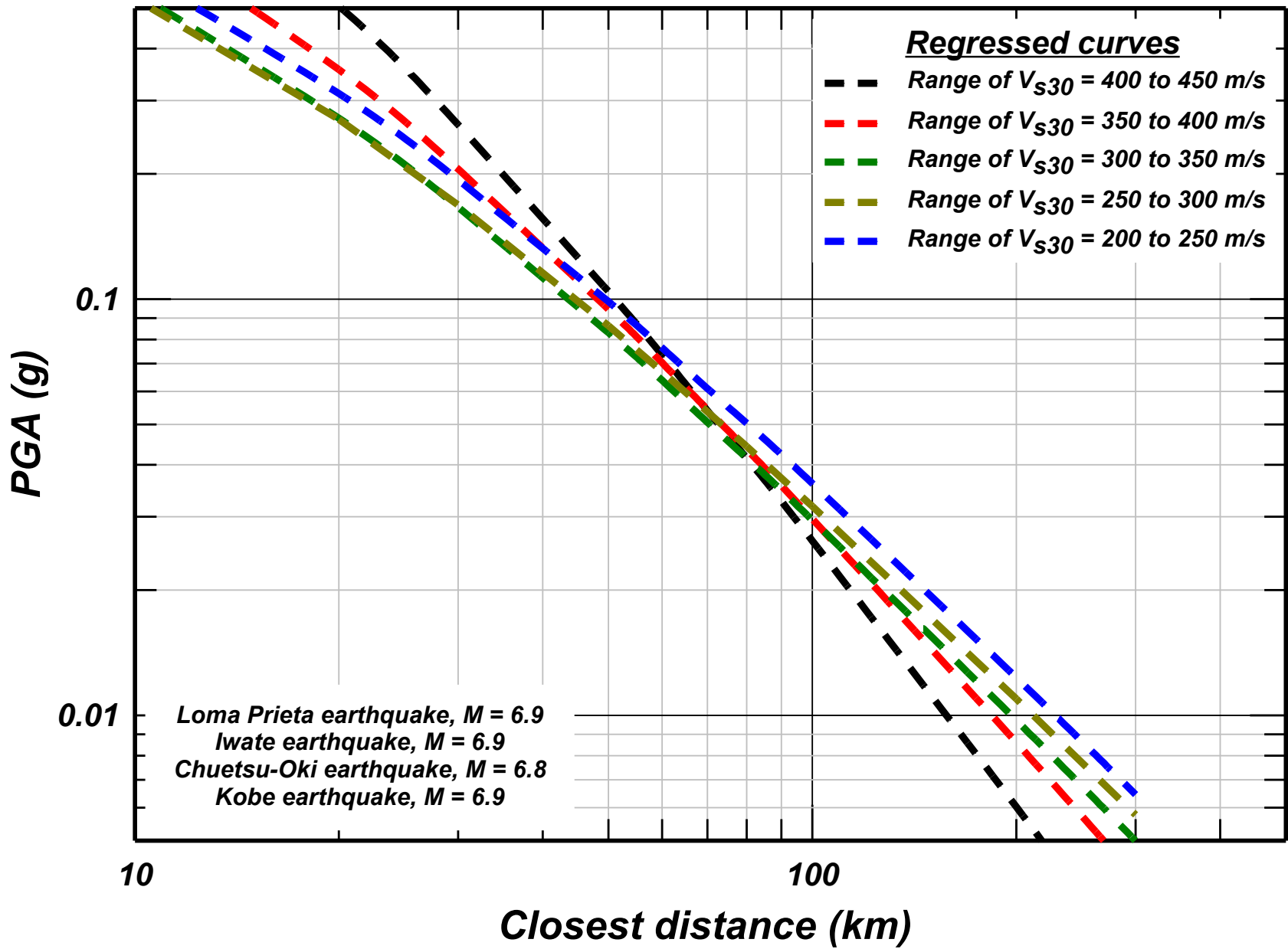












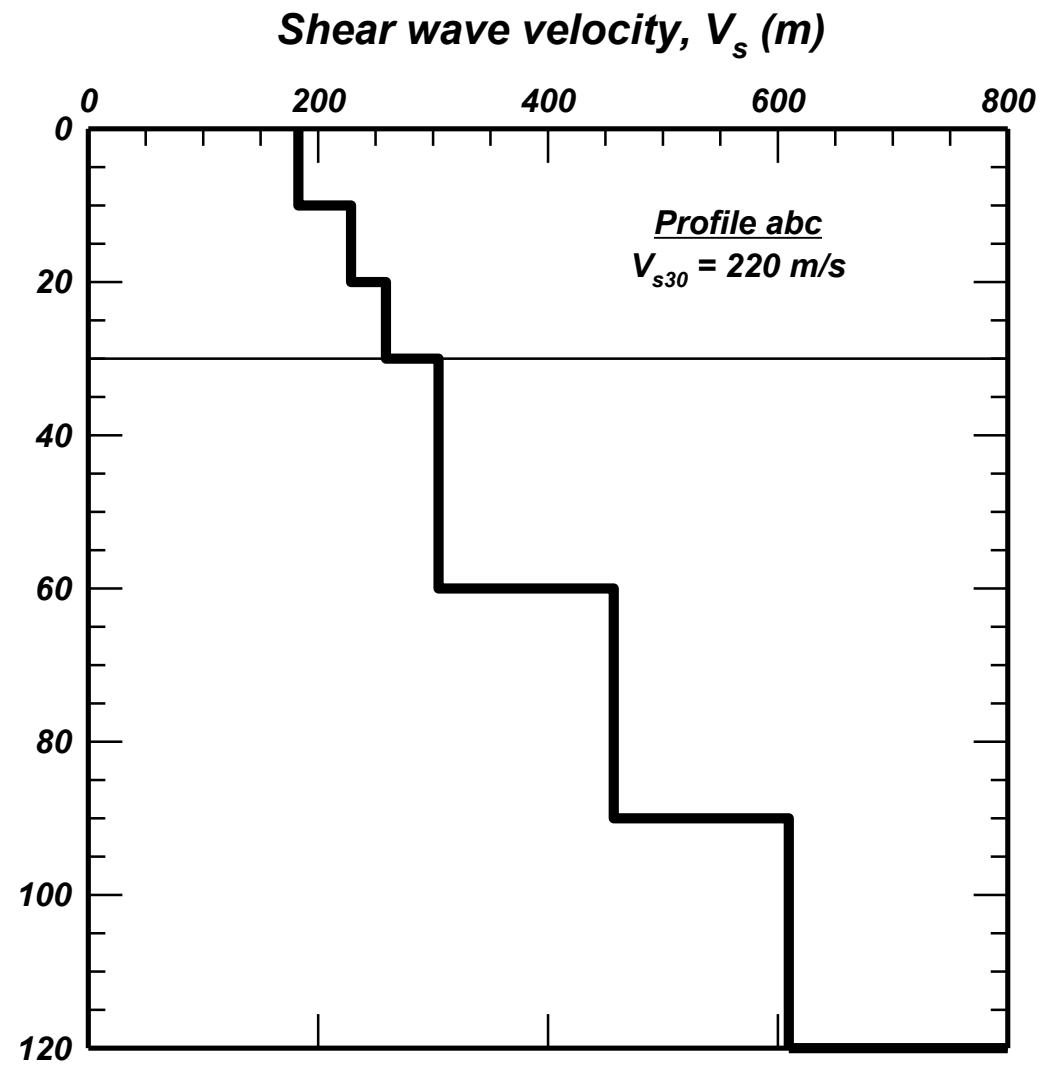
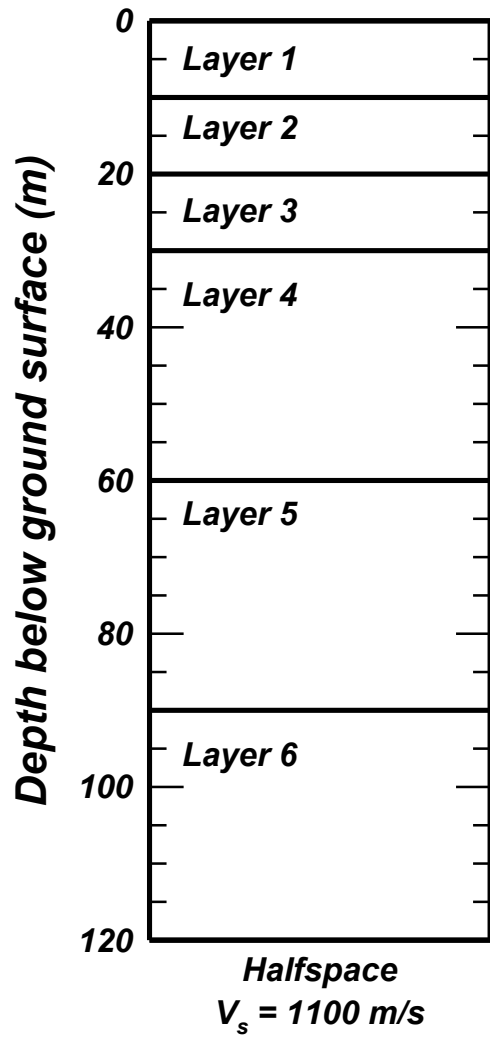
WHAT DO THE NGA DATA SHOW?

***The data generally **do not fully** support the
"published" trends.***

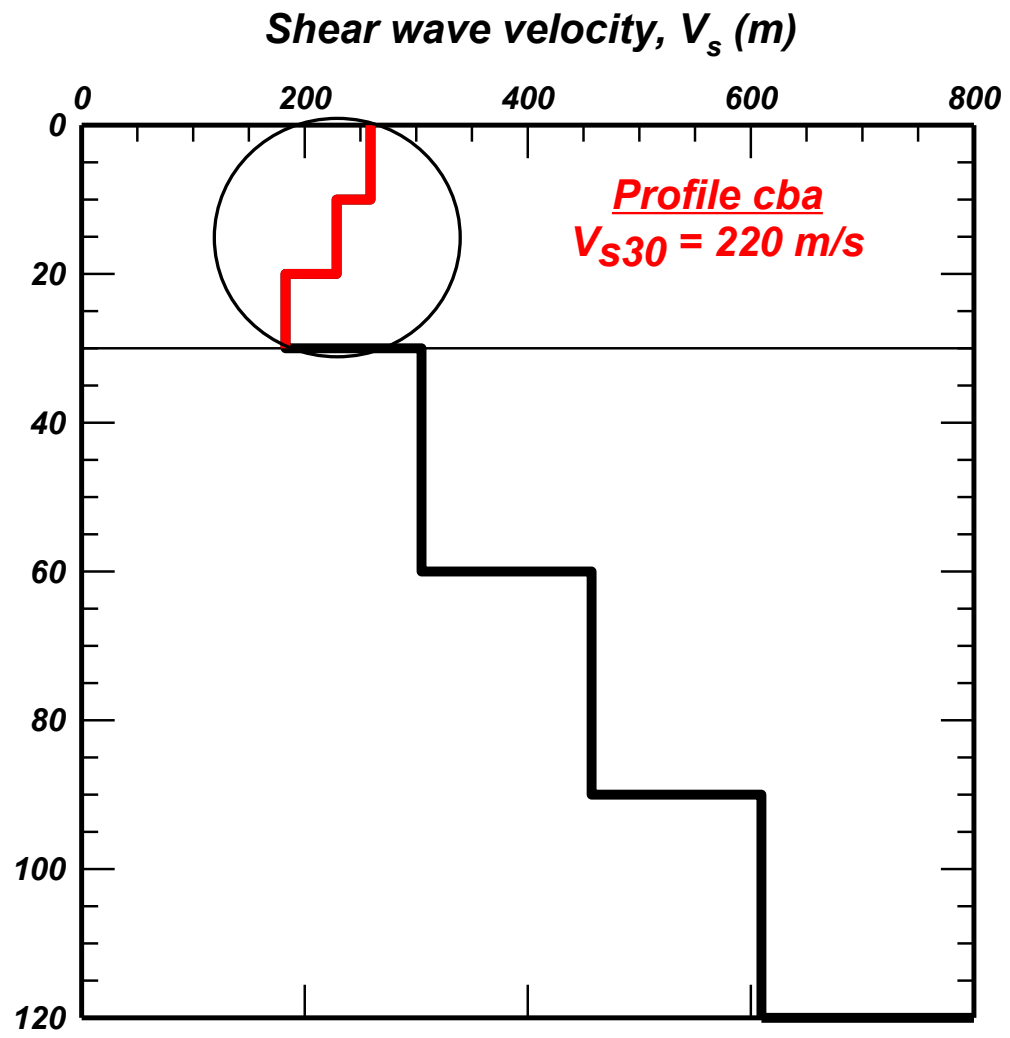
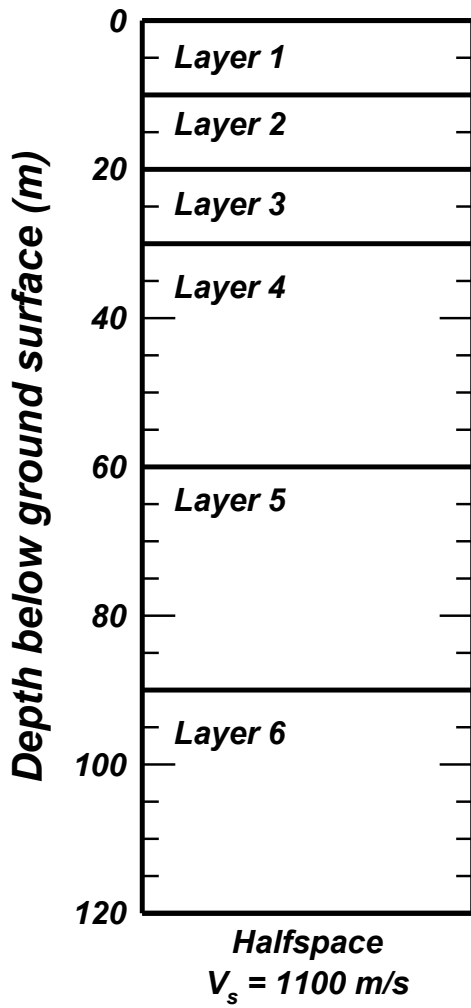


Site Response Studies





Profile abc



CONCLUDING REMARKS

- ✓ V_{s30} is not a fundamental geotechnical parameter
- ✓ V_{s30} is not a unique geotechnical parameter
- ✓ Since G/G_{max} is material-dependent
- ✓ V_{s30} is neither necessary nor sufficient to describe or accommodate nonlinear effects

CONCLUDING REMARKS

- ✓ *The contributions of the soil profile below 30 m to site response, cannot be accommodated with the use of V_{s30} with or without including the depth to $V_s = 1$ km/s or to $V_s = 2.5$ km/s (even if these depths are known for a sufficient number of sites).*
- ✓ *Sites with "identical" V_{s30} , but differing layering, can have significantly different response*

CONCLUDING REMARKS

- ✓ *Additional work is needed before V_{s30} should be used as a continuous independent parameter in earthquake ground motions attenuation relationships.*
- ✓ *The use of a range of V_{s30} to describe a generalized "site category" for building code purposes, is reasonable.*

CONCLUDING REMARKS

- ✓ **Site-specific response calculations (with at least 7 rock outcrop input motions) are preferable for assessing local site effects – *this requires high quality site response calculations.***
- ✓ **Distance dependence *can be* critical – further studies are in progress, incorporating V_{s30} in estimating the slope of the attenuation relationship.**

STAY TUNED

THANK YOU