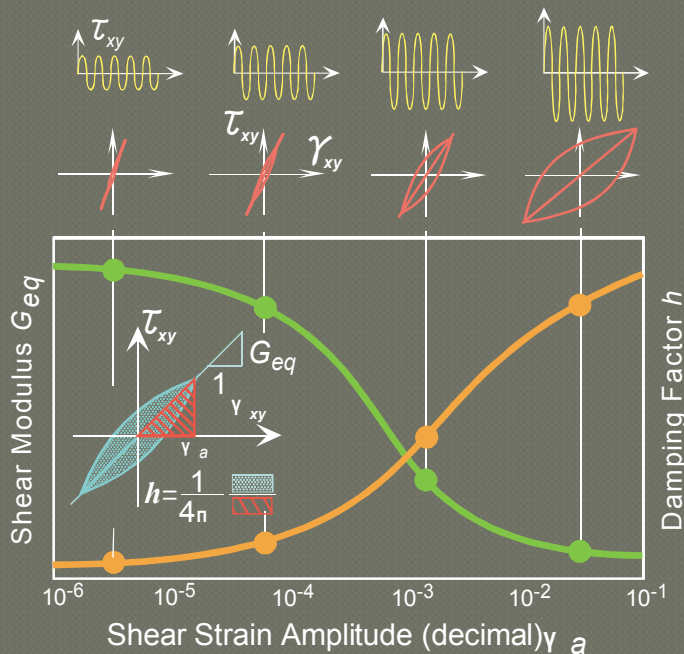


# Nonlinearity in Soil Response: Nonlinear Volumetric Mechanism

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Disaster Prevention Research Institute  
Kyoto University

# Soil non-linearity: Isotropic (equivalent) linear materials



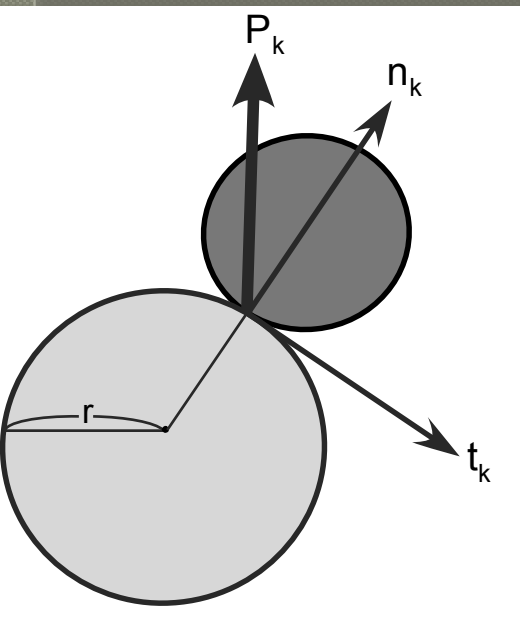
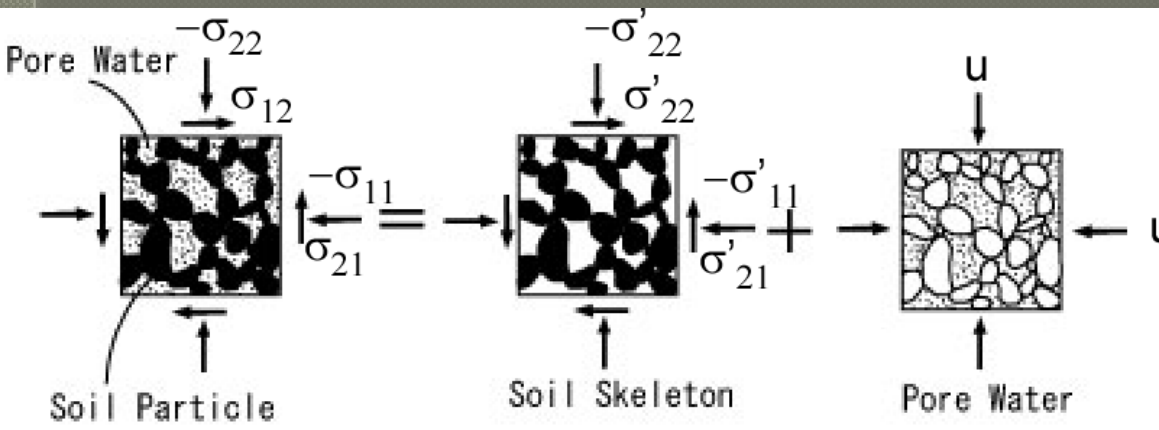
$$\boldsymbol{\sigma} = -p\mathbf{I} + \mathbf{q}$$

$$p = -K\mathbf{I} : \boldsymbol{\varepsilon}$$

$$\mathbf{q} = 2G \left( \boldsymbol{\varepsilon} - \frac{1}{3} \mathbf{I} \otimes \mathbf{I} : \boldsymbol{\varepsilon} \right)$$

Seed and Idriss (1970)

# Soil non-linearity Granular materials



$$\boldsymbol{\sigma} = \boldsymbol{\sigma}' - u\mathbf{I}$$

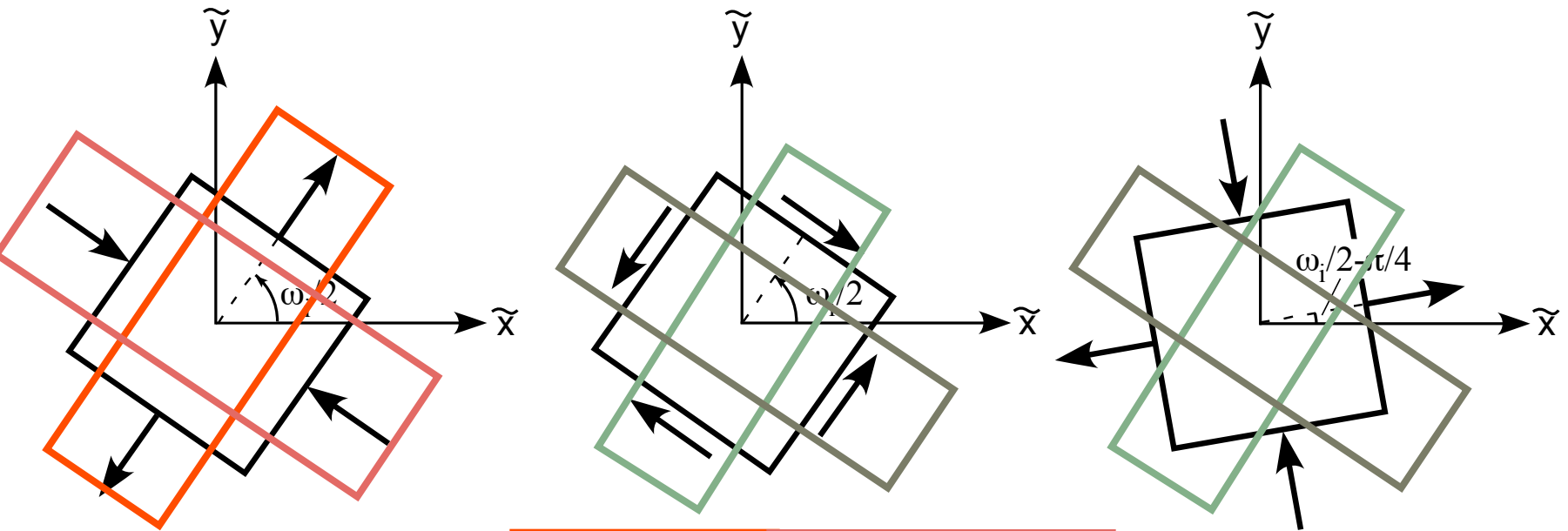
Terzaghi (1943)

$$\mathbf{P} = F\mathbf{n} + S\mathbf{t}$$

Oda (1974)

$$\boldsymbol{\sigma}' = \frac{1}{V} \sum l (F\mathbf{n} \otimes \mathbf{n} + S\mathbf{t} \otimes \mathbf{n})$$

# Virtual shear mechanism



$$\langle \mathbf{n} \otimes \mathbf{n} \rangle = \mathbf{n} \otimes \mathbf{n} - \mathbf{t} \otimes \mathbf{t}$$

$$\langle \mathbf{t} \otimes \mathbf{n} \rangle = \mathbf{t} \otimes \mathbf{n} + \mathbf{n} \otimes \mathbf{t}$$

$$\boldsymbol{\sigma}' = -p\mathbf{I} + \frac{1}{4\pi} \iint q \langle \mathbf{t} \otimes \mathbf{n} \rangle d\omega d\Omega$$

$$\boldsymbol{\varepsilon} = \mathbf{I} : \boldsymbol{\varepsilon}, \quad \gamma = \langle \mathbf{t} \otimes \mathbf{n} \rangle : \boldsymbol{\varepsilon}, \quad \boldsymbol{\varepsilon}' = \boldsymbol{\varepsilon} - \boldsymbol{\varepsilon}_d$$

$$dp = -K_{L/U} d\varepsilon'$$

$$dq = G_{L/U} d\gamma$$

Coupling through dilatancy

Anisotropy

(Beyond equivalent linear analysis)

Iai (1993)

$$d\boldsymbol{\sigma}' = \mathbf{C} : d\boldsymbol{\varepsilon}'$$

$$\mathbf{C} = K_{L/U} \mathbf{I} \otimes \mathbf{I} + \frac{1}{4\pi} \iint G_{L/U} \langle \mathbf{t} \otimes \mathbf{n} \rangle \otimes \langle \mathbf{t} \otimes \mathbf{n} \rangle d\omega d\Omega$$

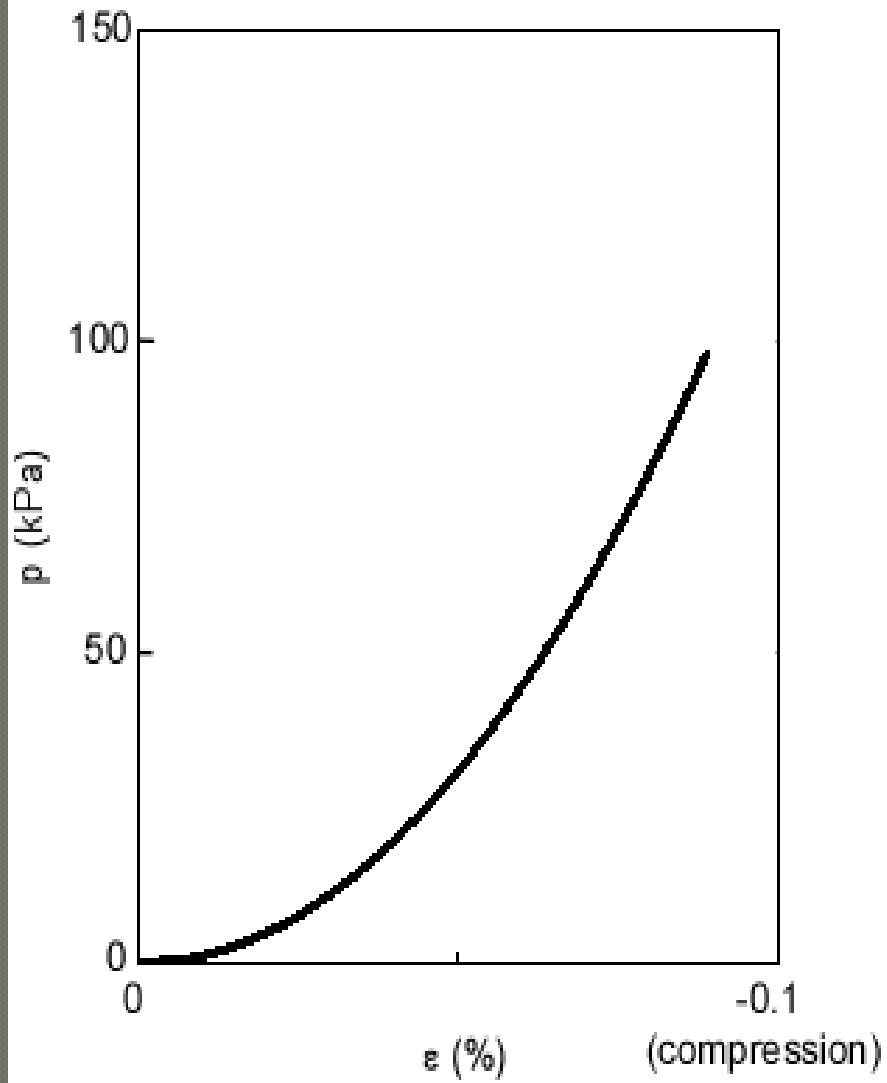
$$d\boldsymbol{\varepsilon}' = d\boldsymbol{\varepsilon} - \frac{1}{3} d\varepsilon_d \mathbf{I}$$

# Nonlinear Volumetric Mechanism

$$K_{L/U} = K_a \left( \frac{p}{p_a} \right)^{n_K} \quad \text{for } p \geq 0 \text{ (compression)}$$

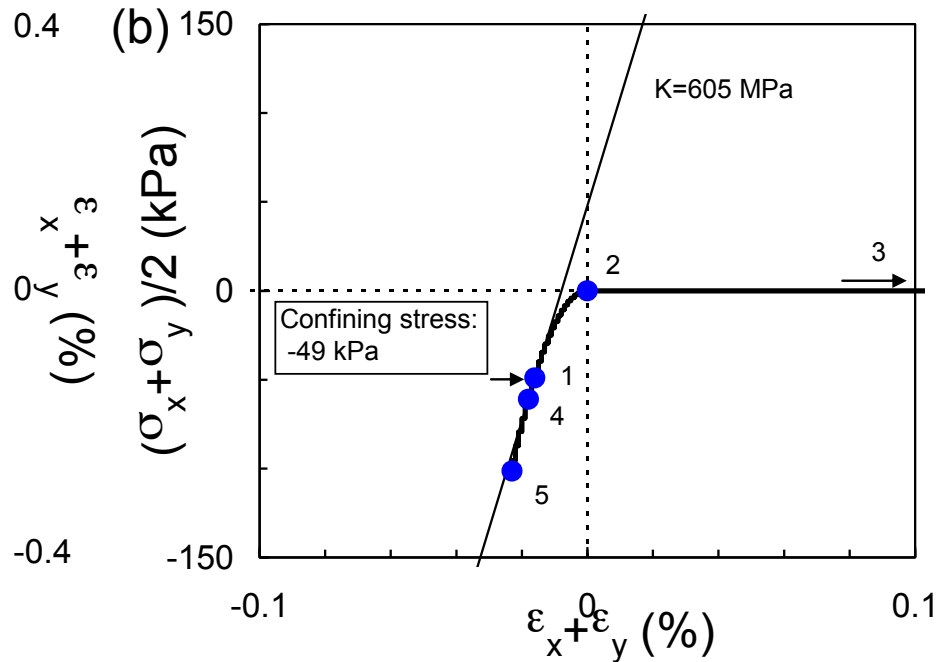
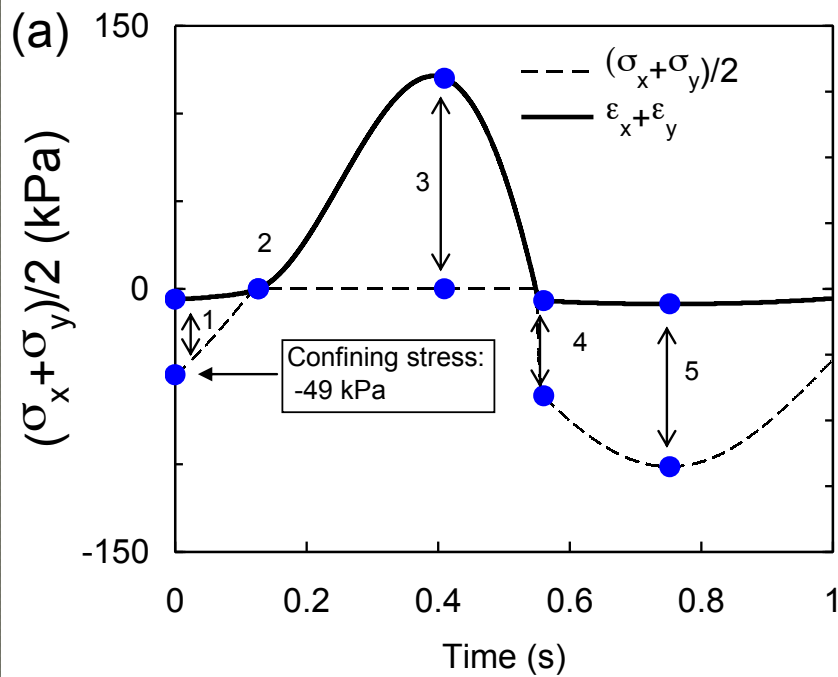
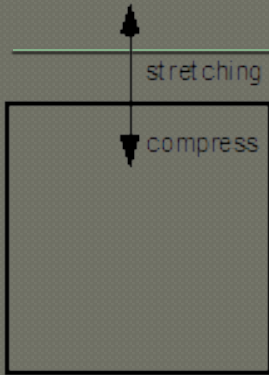
$$p = \begin{cases} p_a \left( - (1 - n_K) \frac{\varepsilon'}{\varepsilon_{ma}} \right)^{\frac{1}{1-n_K}} & \text{for } \varepsilon' < 0 \text{ (compression)} \\ 0 & \text{for } \varepsilon' \geq 0 \text{ (extension)} \end{cases}$$

$$\varepsilon_{ma} = \frac{p_a}{K_a}$$

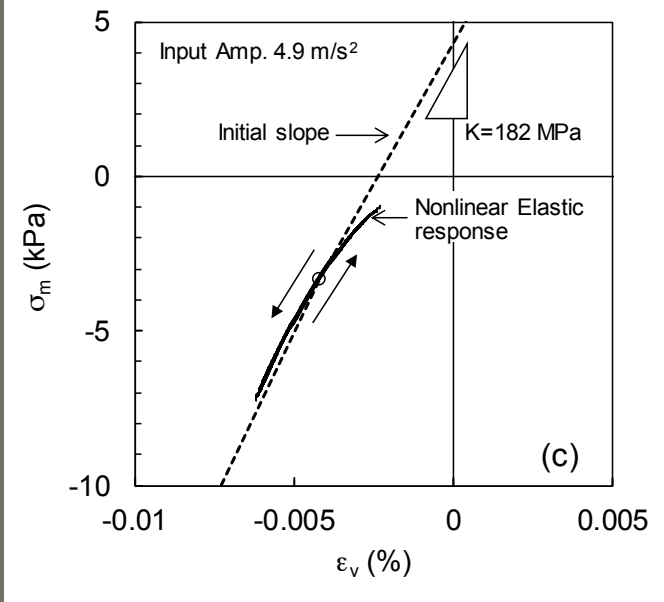
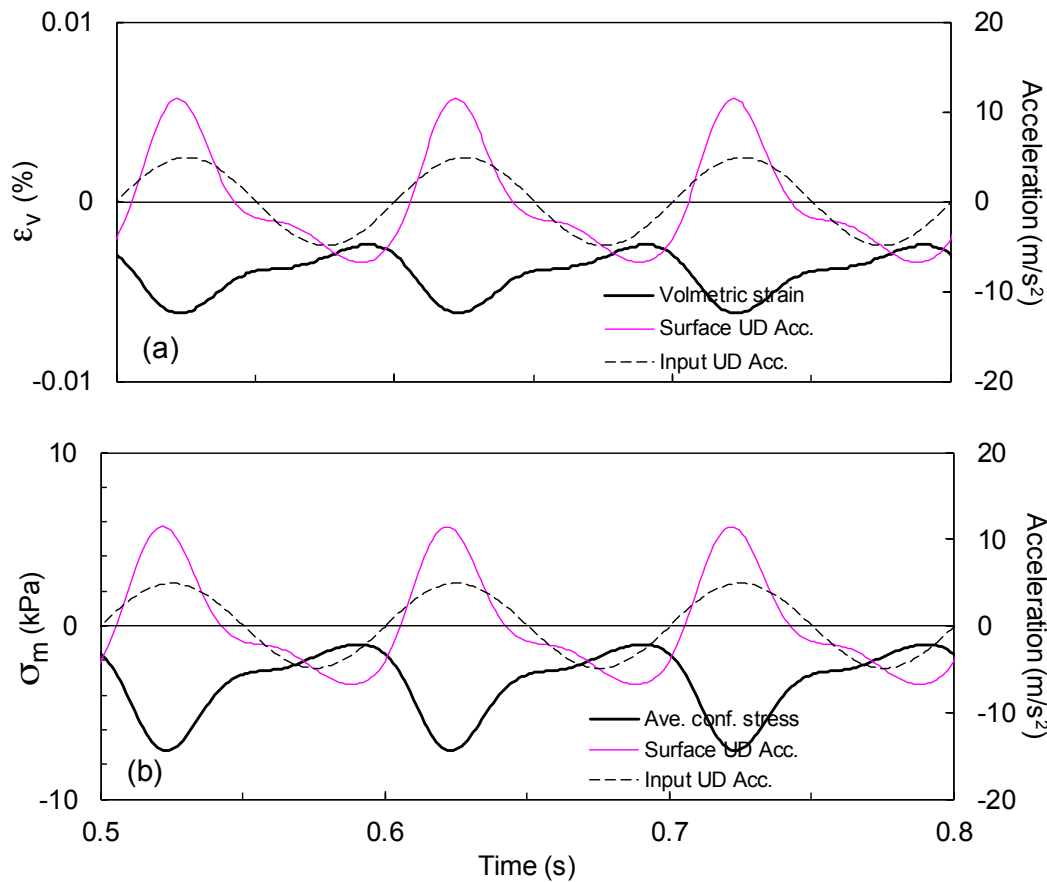




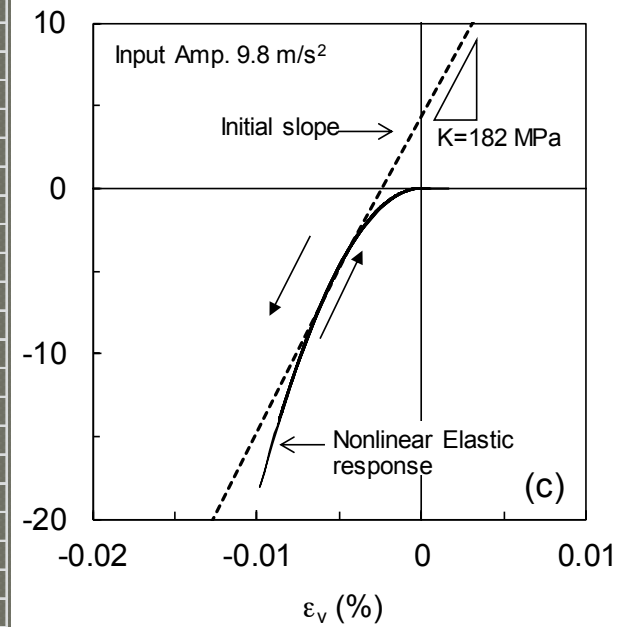
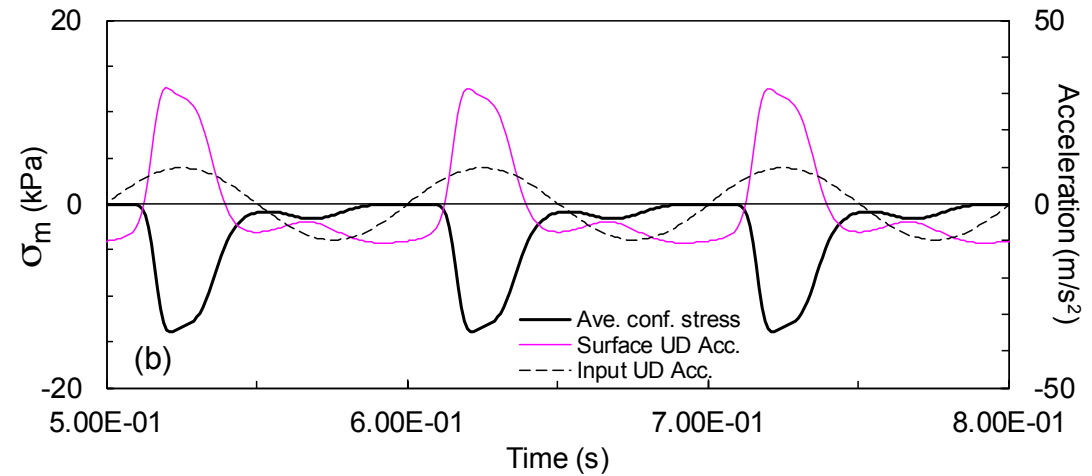
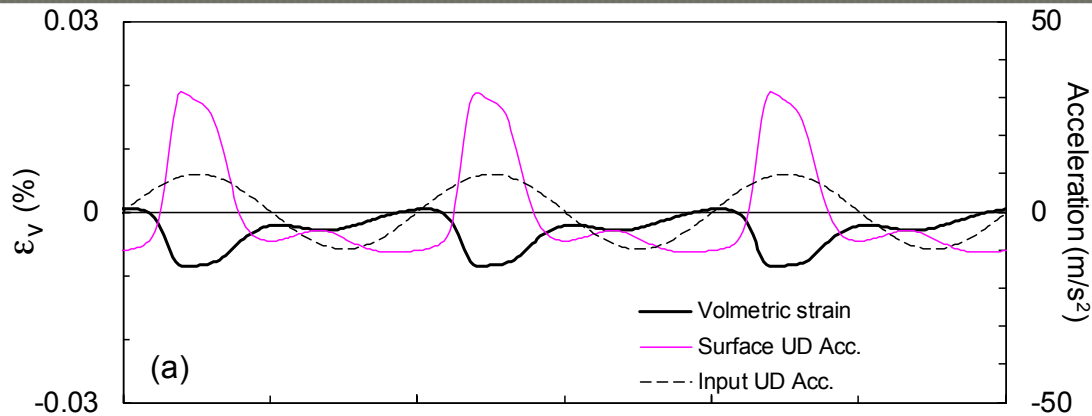
# Model Behavior under Cyclic Vertical Stretching and Compression



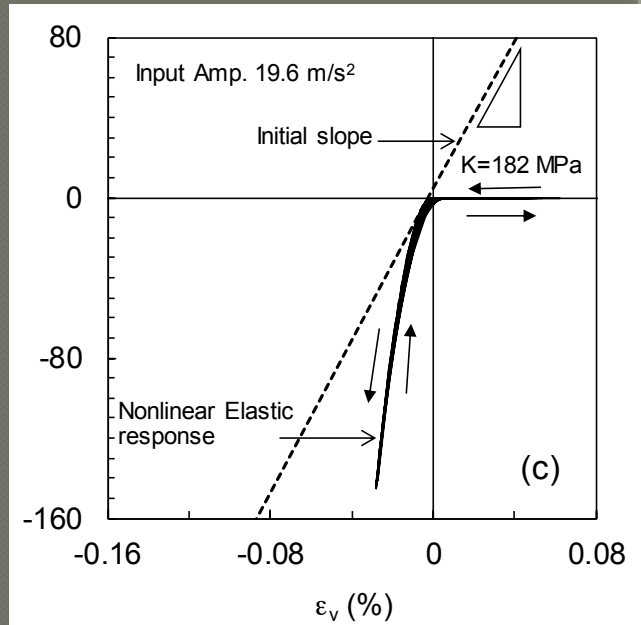
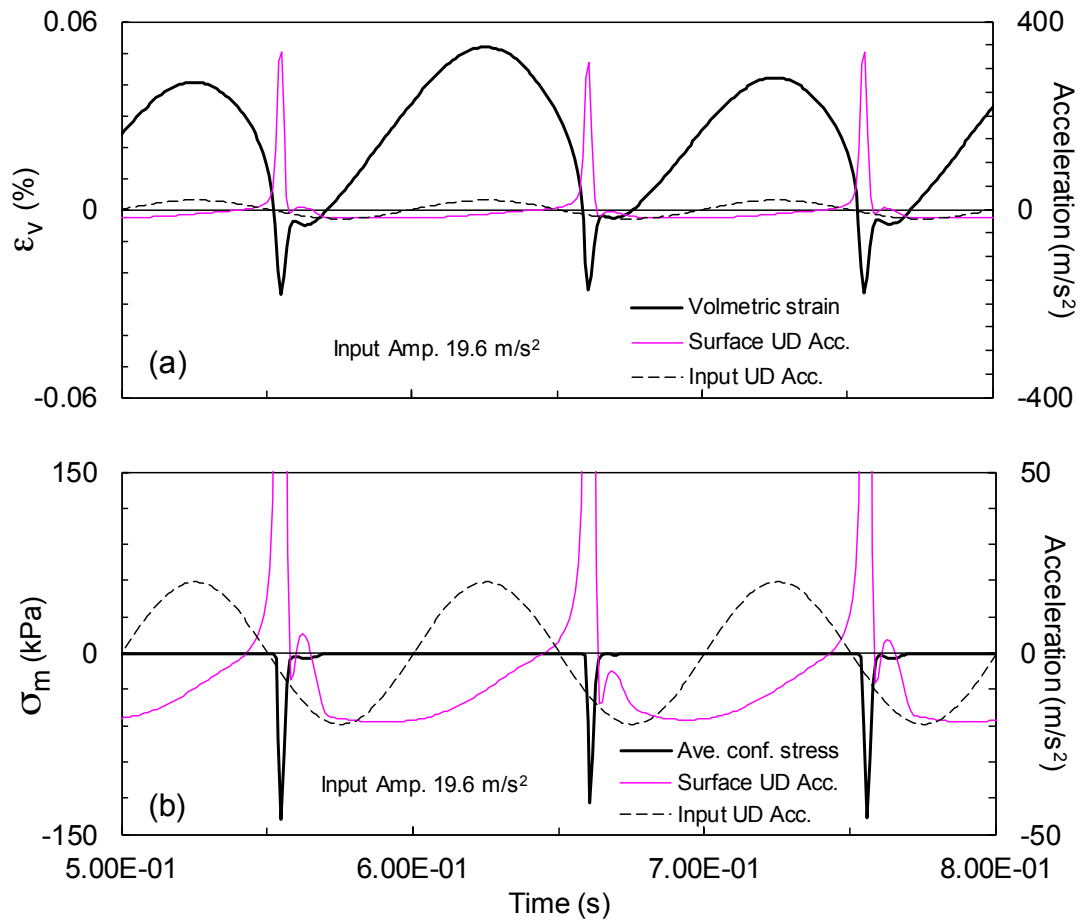
# Model Behavior under cyclic Vertical Input Acceleration (0.5g)



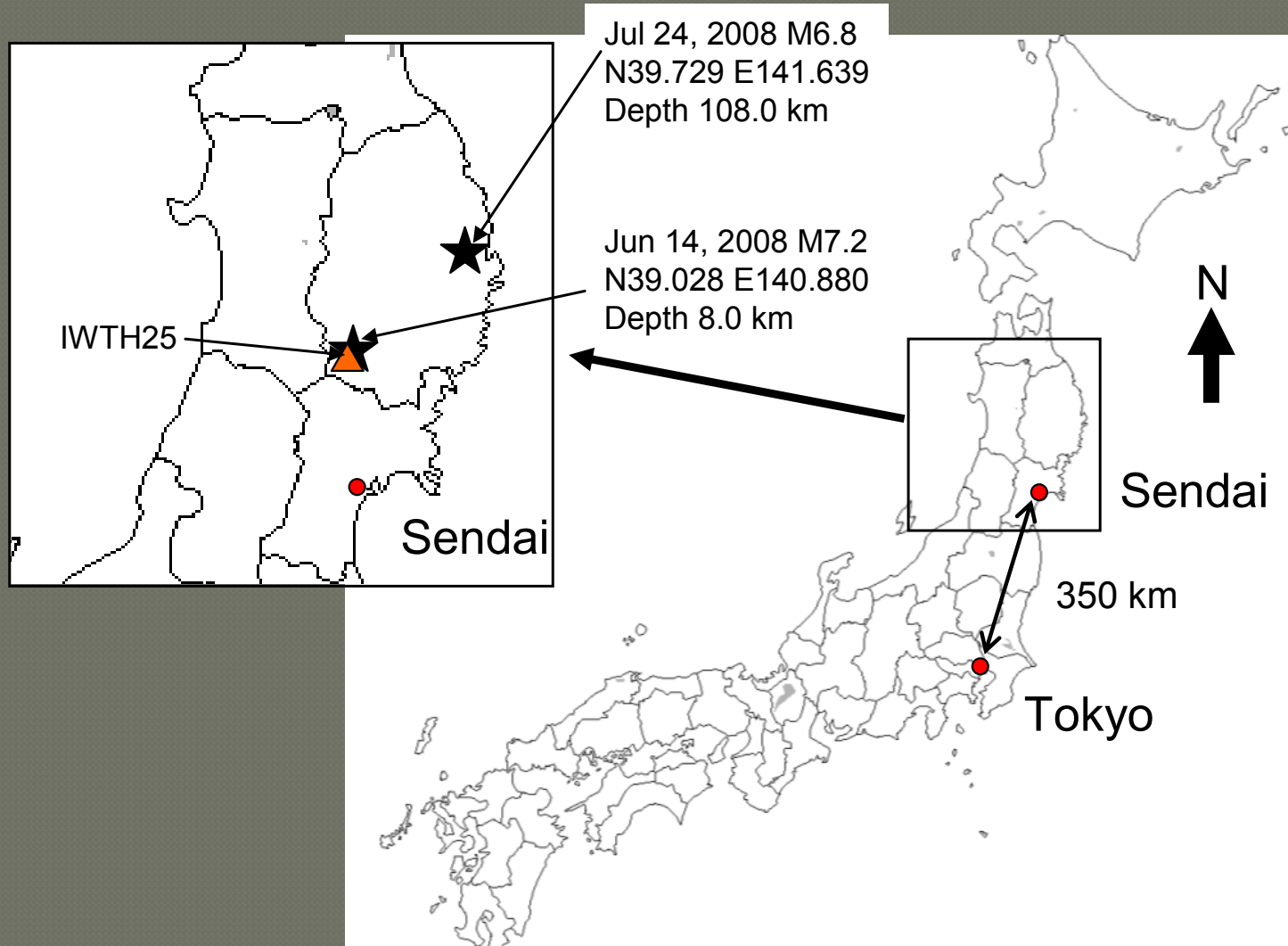
(1g)

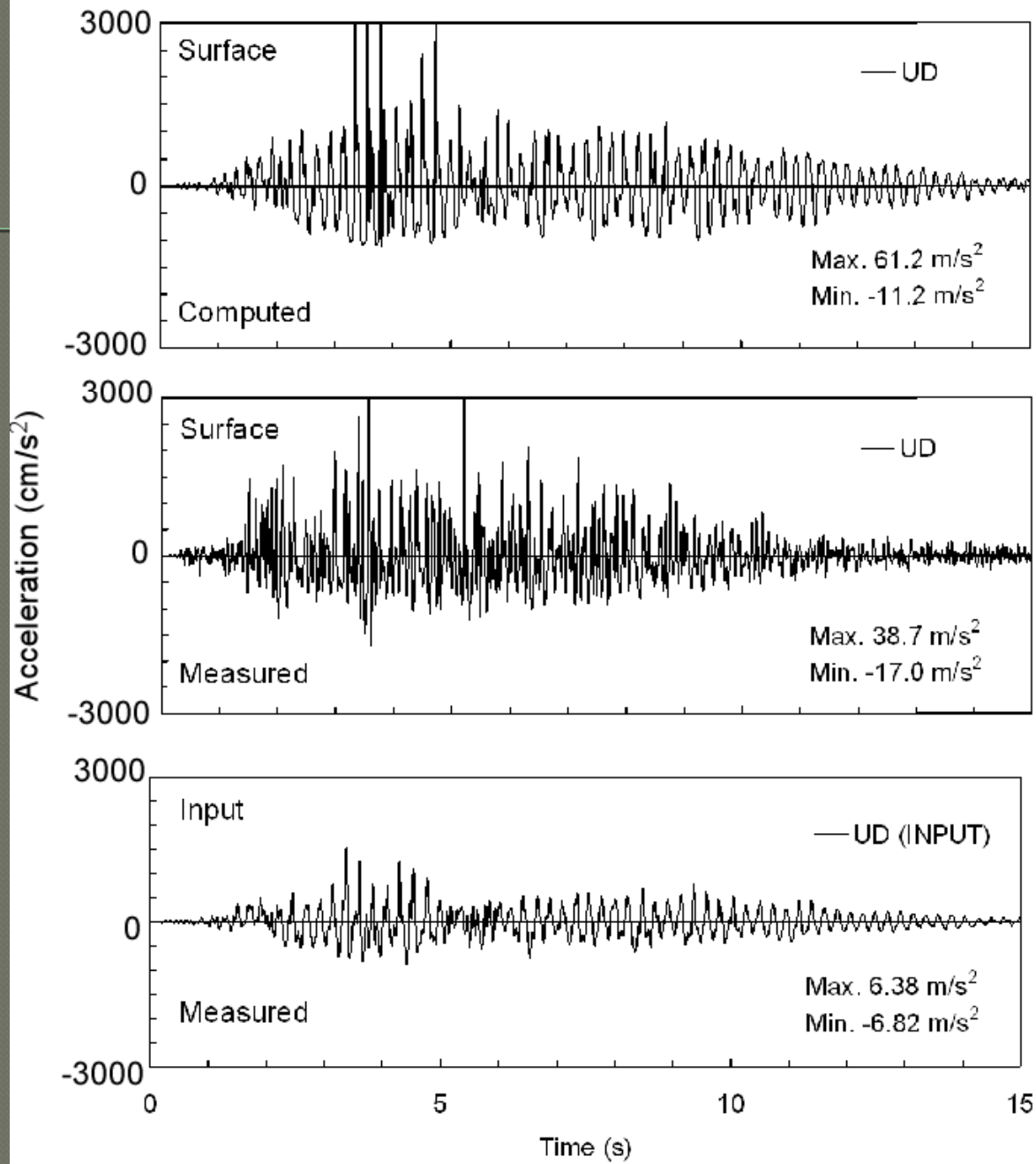


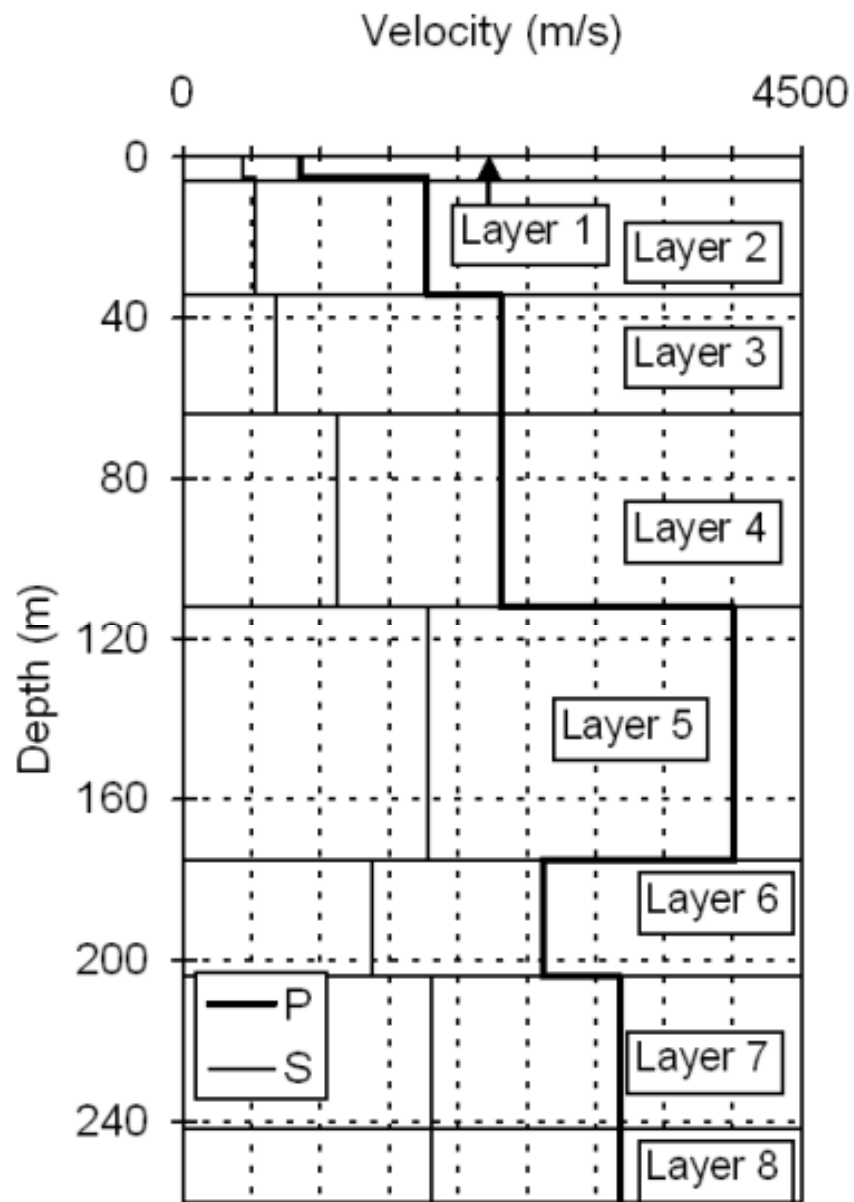
(2g)

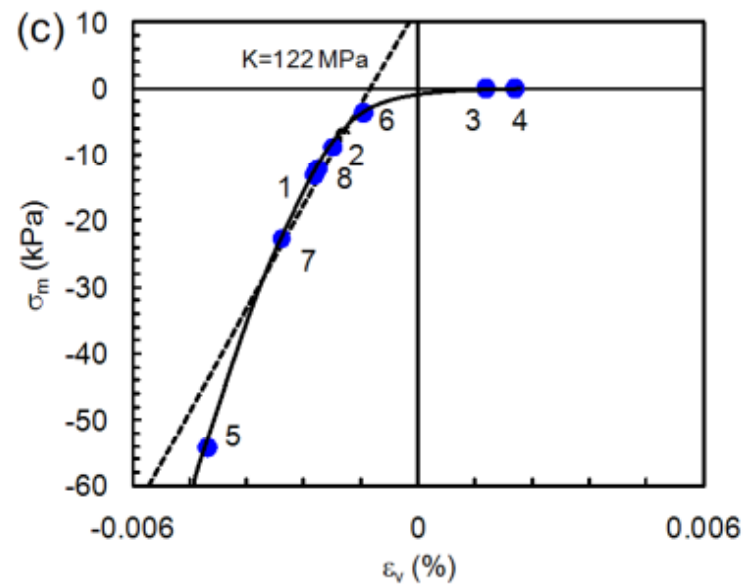
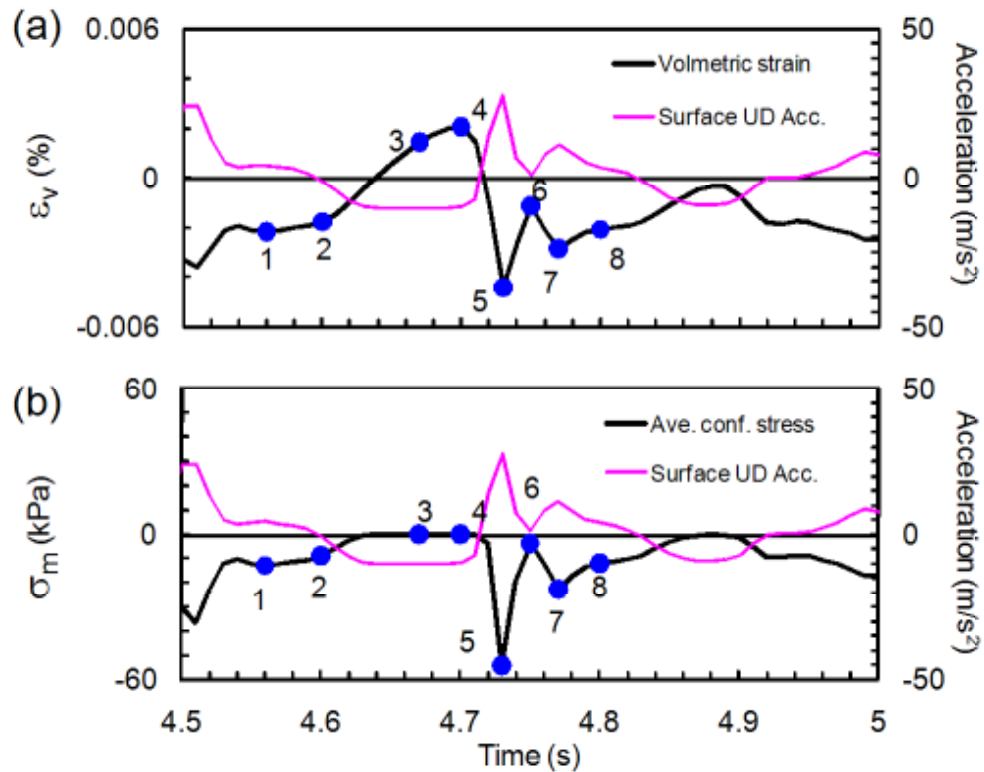


# Nonlinear Volumetric Mechanism: Evidence from the Field



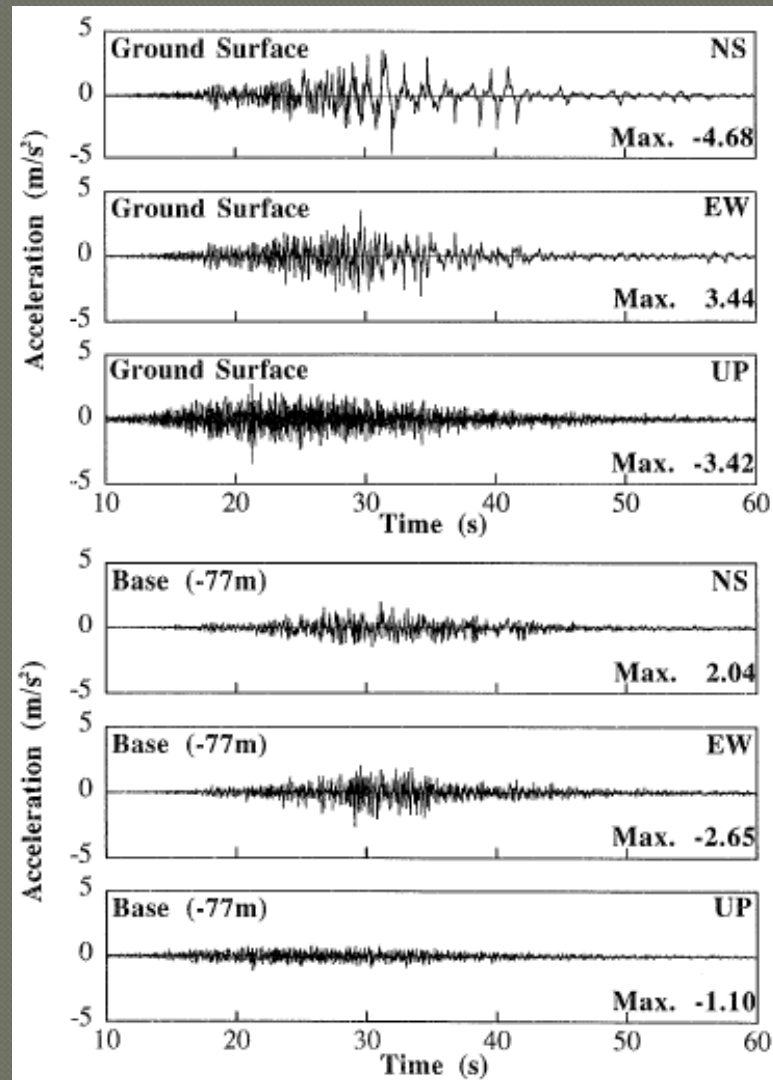


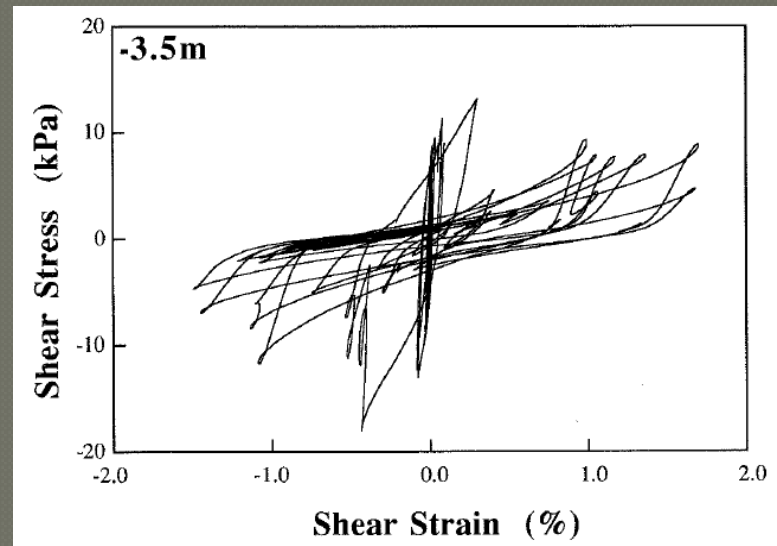
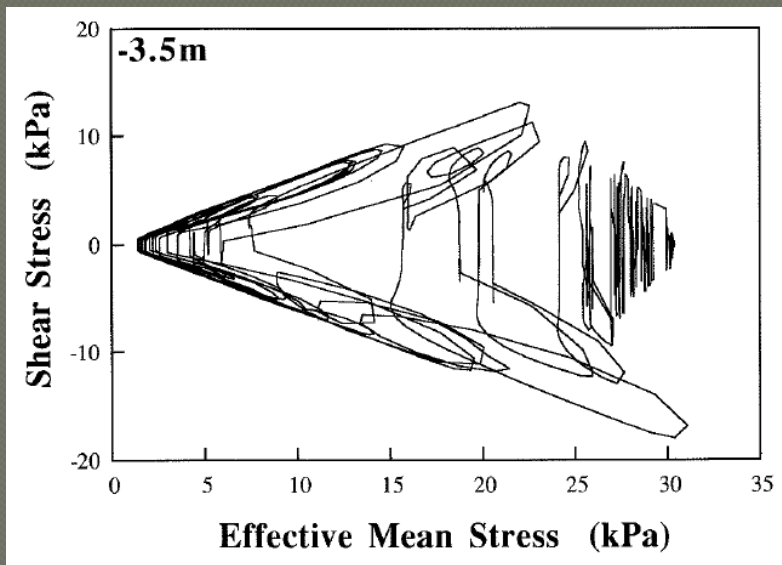
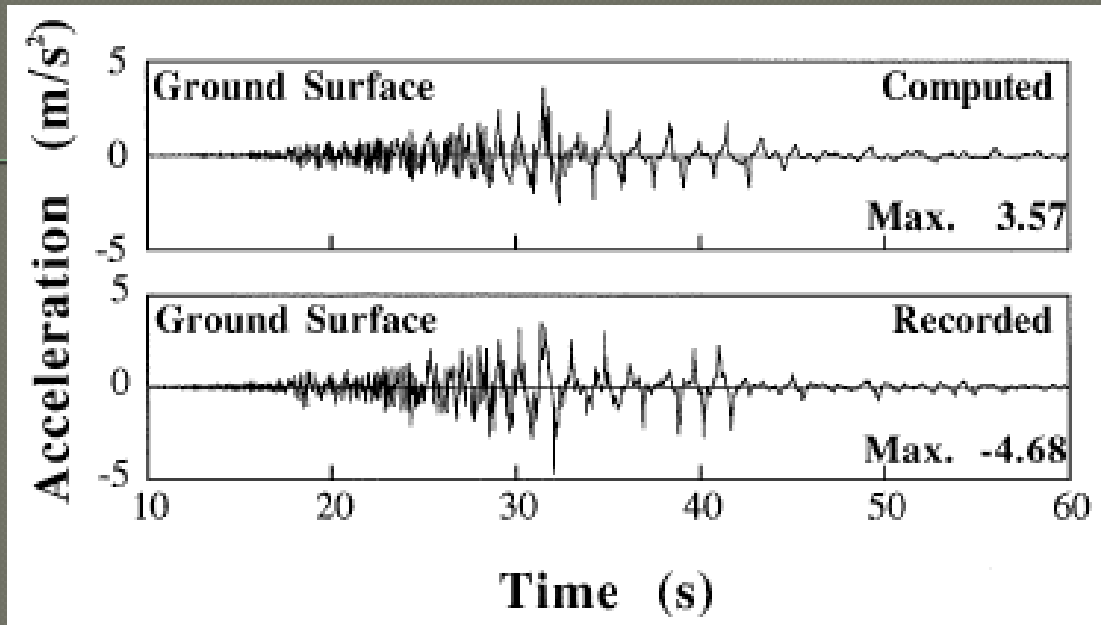




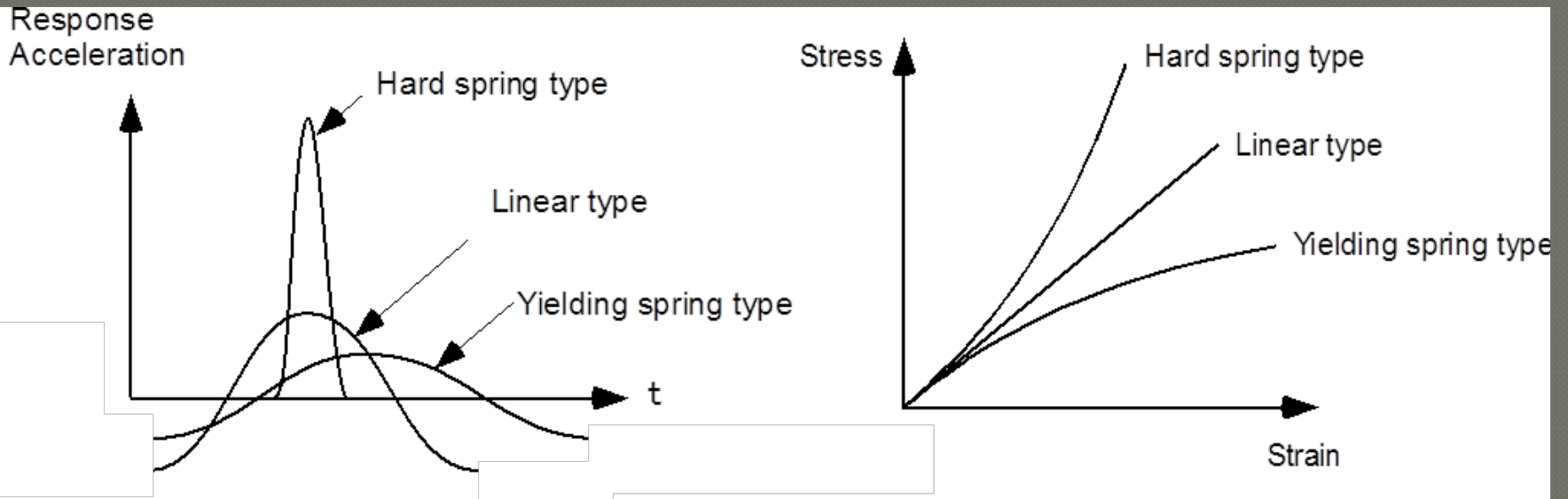


# Mechanism of Spikes in Site Response





# Nonlinearity



# Conclusions

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- Gravity → confining stress in the soil
- Strong vertical motion (large volumetric strain) → nonlinear volumetric response
- A peak acceleration of 4.0g (2008 Iwate-Miyagi Inland, Japan, earthquake)
- Nonlinearity of hard spring type → spikes in acceleration